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9 TECHNICAL REPORT ARLCD TR-77062

6 DYNAMICS OF THE PIN PALLET  
RUNAWAY ESCAPEMENT.

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US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND  
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20. The simulation is applied to the timing of the mechanism of the M525 fuze with an assumption of constant input torque to the escape-wheel. The influence of changes on such parameters as escape-wheel torque, pallet moment of inertia, center distance, pallet radius, etc., are explored in detail by appropriate computer runs. Agreement has been found with existing experimental data. Finally, recommendations for continued work are given.

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## INTRODUCTION

It was the aim of the present investigation to develop a realistic and workable computer simulation of the dynamic behavior of the pin pallet runaway escapement which can be used in the analysis and synthesis of various safing and arming devices. This goal has been achieved.

This report describes and formulates the dynamics of the various regimes of motion which form the basis for the simulation. The computer program and its controls are presented in detail. The simulation is applied to the time delay mechanism of the M525 fuze and the influence of various parameter changes is explored. Previous experimentation and practical experience with this mechanism confirmed the results of the computations. Finally, recommendations for continued work are given. The previous work done in this field is listed in references 1-15.

## SIMULATION OF PIN PALLET RUNAWAY ESCAPEMENT

The present effort on the pin pallet escapement represents an extension of the work of M. E. Anderson and S. L. Redmond (ref. 7). New methods of contact kinematics for coupled motion, of contact sensing, and of computational controls are developed.

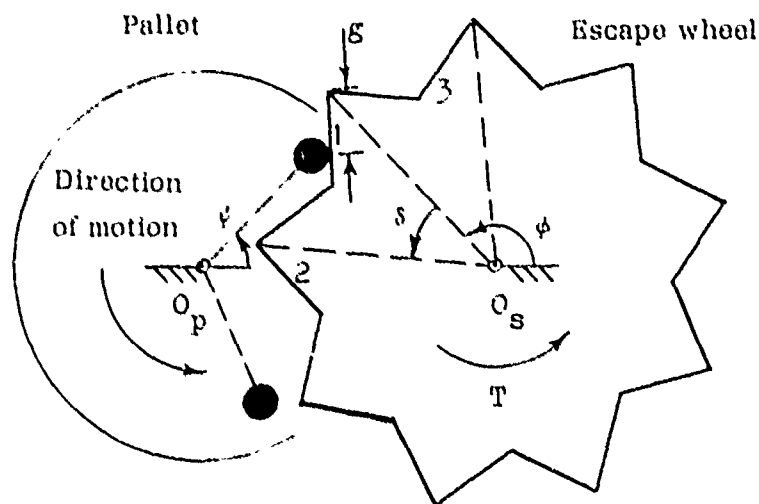


Figure 1. Coupled motion

The following outlines the overall assumptions and derivations for the various regimes of motion. A detailed description of the actual computer program and its controls is then given.

### Coupled Motion

Figure 1 shows the upper pallet pin<sup>1</sup> being driven in coupled motion by tooth no. 1 of the escape wheel (top contact). The escape-wheel angle  $\phi$  is defined by the line from the escape-wheel pivot  $O_s$  to the tip (with-out radius) of the contacting tooth (or the one about to make contact) and the line connecting  $O_s$  to the pallet pivot  $O_p$ . Similarly, the angle  $\psi$ , which is defined by the line from  $O_p$  to the active pallet pin center (top or bottom) and the center line, describes the motion of the pallet. The escape wheel is driven by the constant moment  $T$  in the positive direction of rotation. While it is assumed that friction acts on the pallet pin/escape wheel tooth interface, it is neglected at both pivots since investigation showed that its effects are negligible when the pivots are of the usual small diameter.

The quantity  $g$ , which represents the distance from the contact point to the tip of the escape-wheel tooth, is used to determine the end of coupled motion. Appendix A contains derivations for this expression, as well as all other kinematic quantities associated with coupled motion. Appendix B, with the help of appendix C, gives the derivation of the differential equation of coupled motion in terms of the escape-wheel angle  $\phi$  (eq. B-10).

### Free Motion

When coupled motion is finished (i.e.,  $g = 0$ ) or when separation of contact occurs after impact, the escape wheel and pallet move independently of each other in free motion. Figure 2 shows this free motion for the bottom phase of the action, i.e. the bottom pallet pin is about to make contact with tooth no. 2 of the escape-wheel. The constant torque  $T$  continues to act on the escape-wheel, while the motion of the pallet depends only on its initial conditions. Again, any frictional retarding moments at the pivots are neglected. Position sensing during free motion is based on  $g'$ , the distance of the pallet pin center from the tip of the escape-wheel

<sup>1</sup>This report uses the word upper when referring to entrance motion and lower when referring to exit motion.

tooth (parallel to the face of the tooth) and  $f$ , the distance between the pallet pin and tooth surfaces normal to the tooth). Expressions for these quantities are derived in appendix D. The differential equations for the free motion of the pallet and the escape-wheel are derived in appendix E.

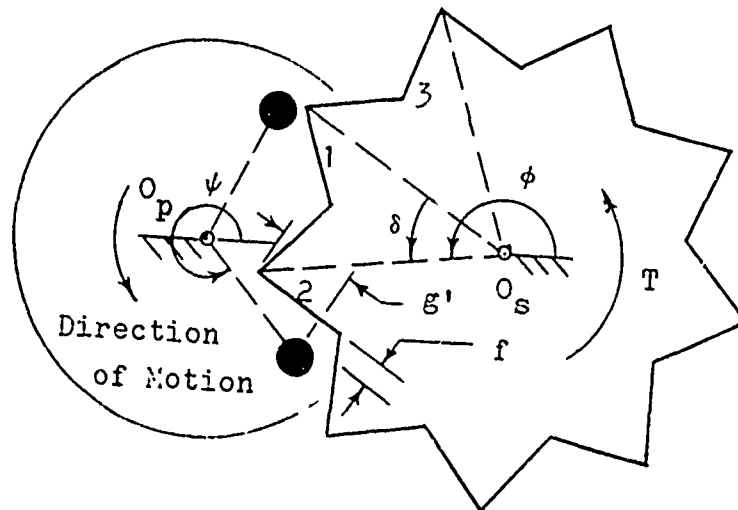


Figure 2. Free motion

### Impact

Impact follows free motion whenever  $f$  equals zero,  $g'$  is smaller than zero, and the relative velocity between the contacting surfaces warrants it. Such an impact usually reverses the motion of the pallet (fig. 3) and under certain circumstances also reverses the motion of the escape-wheel temporarily. While the impact equations, derived in appendix F, allow for both normal and tangential impulses to produce changes in the angular momenta of the pallet and escape-wheel, the computer program presented here neglects the tangential impulse for the sake of simplicity. The classical coefficient of restitution formulation is used to account for the energy loss during impact.

Figure 4 shows free motion for the subsequent top phase of the motion, i.e. the top pallet pin is about to make contact with tooth no. 3 of the escape-wheel.

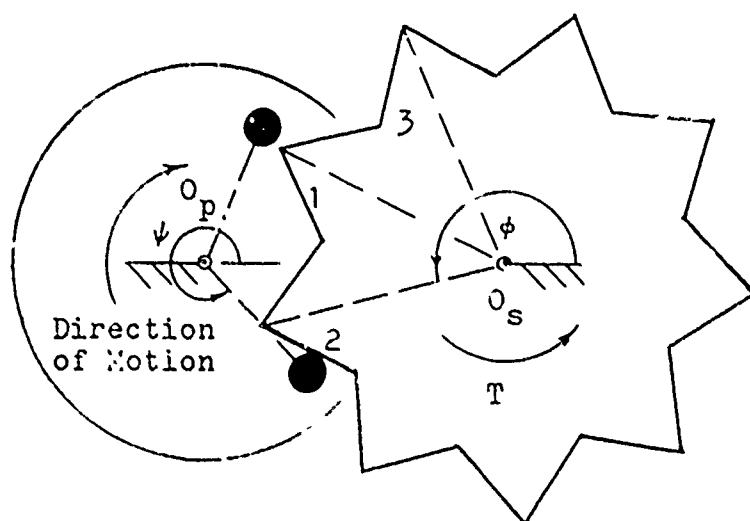


Figure 3. Impact

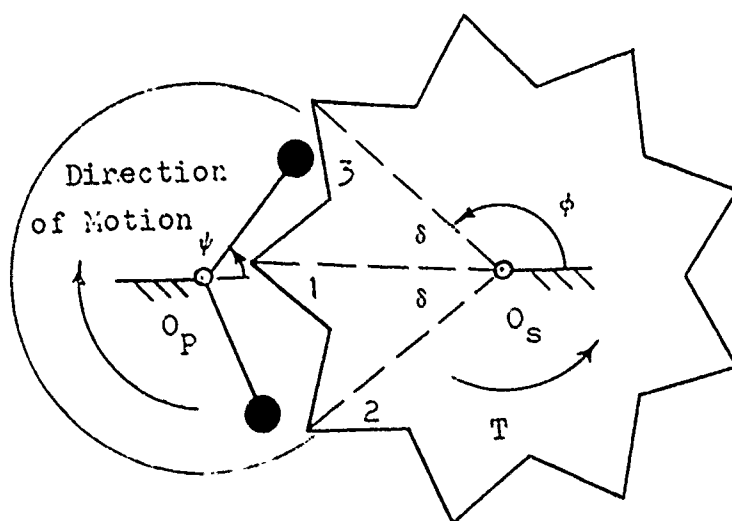


Figure 4. Impending top contact

All kinematic and dynamic expressions are derived in such a manner that they are valid for top and bottom action. The simulation recognizes only contact on the front faces of the escape-wheel teeth. Pathological conditions, such as impact on the tips or the back faces of the escape-wheel teeth are not considered. (The control quantities  $g$  and  $g'$  make it clear that when such a condition exists the computation can be discontinued.)

### Escapement Nomenclature

Figure 5 shows a schematic representation of the pin pallet escapement and indicates its basic geometric nomenclature.

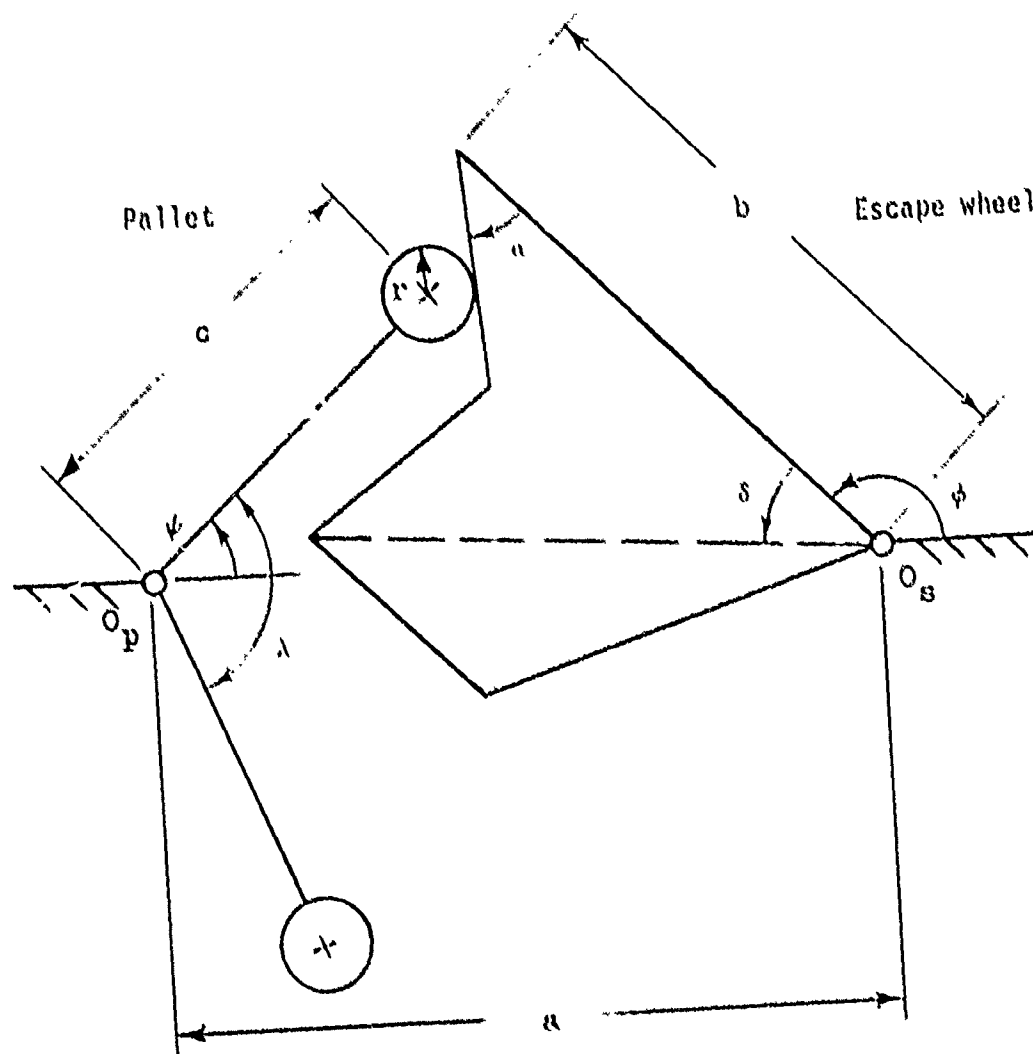


Figure 5. Escapement nomenclature

- $a$  = Distance between pivot points  $O_p$  and  $O_s$
- $b$  = Escape wheel radius
- $c$  = Pallet radius (equal on top and on bottom for simplicity)



- $r$  = Pallet pin radius (equal for top and bottom)
- $\alpha$  = Escape-wheel tooth half angle
- $\delta$  = Angle between escape-wheel teeth
- $\varphi$  = Angular position of escape-wheel
- $\psi$  = Angular position of pallet

### DESCRIPTION OF COMPUTER PROGRAM

The following gives the essential steps of the computer program as listed in appendix G<sup>2</sup>. The flow chart of the program is shown in figure 6. The choice of variable designations was made in such a way that they differ as little as possible from the nomenclature used in the various derivations in appendixes A to F and H.

The main program starts the simulation with top contact coupled motion at a starting angle  $\varphi = 135^\circ$  (called PHID in the computer program) and a cumulative-escape-wheel angle PHITOT of  $0^\circ$ . The choice of this starting angle is connected with the geometry of the example mechanism used ( $\varphi_M = 132.487^\circ$  for the example mechanism).

#### Coupled Motion (location 100)

To solve the differential equation of coupled motion (see equation (B-10) of appendix B) the main program calls on an available fourth-order Runge-Kutta routine.<sup>3</sup> The subroutine FCT computes all needed values and presents the second-order differential equation in terms of two first-order ones to RKGS. PHI (1) and PHI (2) represent the angle  $\varphi$  and the angular velocity  $\dot{\varphi}$ , respectively. The associated subroutine OUTP is responsible for printing out the results of the integration together with the current values of time,  $g$ ,  $\dot{g}$ ,  $\psi$ ,  $\dot{\psi}$ , and PHITOT. In addition, it has the task of deciding whether coupled motion is to be continued. Coupled motion is continued

a. as long as  $g < 0$ . (See equation (A.12) and note, that because of the nature of the coordinate system,  $g$  is always negative while the pallet pin makes contact with the escape-wheel tooth.) And,

<sup>2</sup>The program shown is written in FORTRAN for the CDC System at ARRADCOM, Dover, NJ. It is also available in a slightly modified form for the IBM System/360 at the City College of New York.

<sup>3</sup>RKGS Routine, IBM System/360 Scientific Subroutine Package, (360A-CM-OX3) Version III.



b. for a positive (counterclockwise) rotation of the escape-wheel, if the succeeding absolute value of  $\dot{\psi}$  (DPSI) is larger than the one obtained from the preceding computation (called DPSIP). These values of  $\dot{\psi}$  are computed with the help of equation (A.18), which assumes closure. This condition is necessary, since in coupled motion when  $\dot{\phi}$  is positive the escape-wheel can only drive the pallet, not slow it down. If such a slowdown is indicated, it means that pallet and escape-wheel have separated and free motion will take place. Or,

c. for a negative rotation of the escape-wheel (which may occur after impact), a succeeding absolute value of  $\dot{\psi}$  must be smaller than the preceding one. If for some reason the escape-wheel should speed up and cause the computation to show a larger succeeding value of  $\dot{\psi}$ , it would also serve as an indication that closure has terminated and free motion has started.

To make this process less sensitive, the last two conditions will only be violated when the absolute magnitude  $|\dot{\psi}| \geq 1$  rad/sec.

Thus, when control is returned to the main program, it is either because the pallet pin has left the end of the tooth and there is no further possibility of coupled motion or the pin has disengaged from the inside of the tooth. In either case, free motion results and control is eventually shifted to the subroutine FREE (location 200). This is done directly if  $g < 0$ . In the case that  $g < 0$ , the main program must decide whether the preceding computations have been made for top or for bottom action and whether the next contact will occur on top or on bottom. In the sample mechanism,  $g = 0$  when  $\phi$  is approximately  $146^\circ$  for top action and approximately  $207^\circ$  for bottom action. (The values of  $\phi_0$  for top and bottom action are located in the section on the example mechanism). If  $\phi \leq 150^\circ$ , all possibility for top contact is ended and  $\phi$  must be incremented by the tooth angle  $\delta$  (see figures 2 and 5), while  $\psi$  must be incremented by the angle  $(2\pi - \lambda)$ . For  $\phi > 150^\circ$ , top contact is expected at the end of bottom action and  $\phi$  must be decremented by the angle  $2\delta$  (see figure 4, where the new top tooth no. 3 comes into action). At the same time, the pallet angle  $\psi$  must be decremented by  $(-2\pi + \lambda)$ . These indexing operations have no effect on the continuous computation of the cumulative escape-wheel angle PHITOT.

### Free Motion (Location 200)

After transferring the initial values for time, angles, and angular velocities from the main program, the subroutine FREE computes the subsequent positions and angular velocities of pallet and escape-wheel in free motion according to equations (E.2), (E.3), and (E.7) and (E.8), respectively, for time increments of  $10^{-5}$  seconds. In addition to the above variables, PHITOT is also continually computed and caused to be printed out. The decision, whether or not to remain in this subroutine, is made with the help of the sensing variables,  $f$  (according to equation (D-7)) and  $g'$  (according to equation (D-11) and now called GP).

If  $f > 0$  and  $g' \leq 0$ , free motion is continued without indexing. If  $f > 0$  and  $g' > 0$ , free motion is also continued, but since contact is no longer possible for the component pair for which the previous computations were made, indexing takes place. This is accomplished in the same manner as described before.

If  $f < 0$ , control is returned unconditionally to the main program. If it finds that  $g' > 0$ , indexing takes place and control is given back to the subroutine, FREE. When  $f \leq 0$ , contact is about to take place or has just occurred. The program must decide whether this contact just represents a close approach, which will be followed by further free motion, whether it represents an impending impact, or whether it is the beginning of coupled motion. To this end, the quantities  $V_p$  and  $V_s$  (see equations (F.22) and (F.23)) are computed for the top and bottom free-motion tests.<sup>4</sup> The first three cases of the top free motion test of the main program are illustrated in figure 7. With both angular velocities ( $\dot{\phi}$  is PHI (2) and  $\dot{\psi}$  is DPSI) positive, the following three possibilities exist:

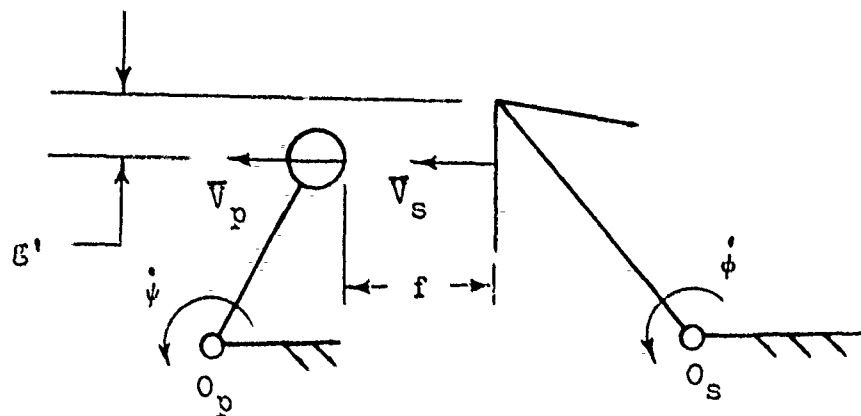
1. If  $|V_p| > |V_s|$ , the contacting surfaces will separate again, free motion will result, and control must be transferred to subroutine FREE (location 200).

2. If  $|V_p| = |V_s|$ , the escape-wheel will start driving the pallet in coupled motion, and control must be transferred to subroutine RKGS (location 99 initiates RKGS).

<sup>4</sup>Under the present circumstances, if  $\phi < 150^\circ$ , only top contact can follow; if  $\phi > 150^\circ$ , bottom contact will occur.

3. If  $|V_p| < |V_s|$ , impact will occur, and control must be given to subroutine IMPACT (location 300).

The remainder of the top free motion tests and the bottom free motion tests are constructed along similar lines for different combinations of angular velocity directions.



( $\dot{\phi}$  and  $\dot{\psi}$  are positive. Distance  $f$  is enlarged.)

Figure 7. Top free motion test

### Impact (Location 300)

The subroutine IMPACT uses the current values of the angular velocities  $\dot{\phi}_i$  and  $\dot{\psi}_i$  and computes the post impact angular velocities  $\dot{\phi}_f$  and  $\dot{\psi}_f$ , applying equations (F.20) and (F.21). (Note that the tangential impact has been neglected and, therefore,  $E_2 = D_1$  and  $F_2 = A_1$ ).

After control is returned to the main program, it is decided whether free or coupled motion follows the impact. This is accomplished by considering the post-impact contact point velocities,  $V_p$  and  $V_s$ , in the impact tests, which are similar to the free motion tests.

If the contact velocities are vectorially equal to each other or if the absolute value of the difference of their absolute magnitudes is less than 2.0 in/sec (5.08 cm/sec), control is transferred to coupled motion. If these velocities are such that they indicate a subsequent separation, which is more usual, computation is transferred to free motion.

The computation is terminated when either  $t = .1$  seconds or when  $\text{PHITOT} \geq 315^\circ$ . These conditions are related to the sample mechanism which runs less than .1 seconds for  $310^\circ$  of escape-wheel rotation.

### EXAMPLE MECHANISM

The pin pallet escapement of the M525 fuze is used as the example mechanism. The following, first, gives the dimensions of the basic escapement (standard configuration) and then discusses certain other data and computed values which are of importance in the computer simulation.

#### Dimensions of the Mechanism

The standard geometric configuration has the following dimensions:

- a = .1931 inches (mean center distance) (.4905 cm)
- b = .15838 inches (.40229 cm)
- c = .09683 inches (.24595 cm)
- r = .01365 inches (.03467 cm)
- $\alpha = 40^\circ$

$$\begin{aligned}
\beta &= 60^\circ \text{ (see figure H-1 in appendix H)} \\
\lambda &= 109.337^\circ \\
\delta &= 40^\circ \\
N &= 9 \text{ (number of teeth of escape-wheel)} \\
I_P &= .91 \times 10^{-7} \text{ lb-sec}^2\text{-in. (moment of inertia IPAL of pallet)} \\
&\quad (1.03 \times 10^{-8} \text{ N - sec}^2\text{-m}) \\
I_S &= .17 \times 10^{-7} \text{ lb-sec}^2\text{-in. (moment of inertia ISTAR of} \\
&\quad (1.92 \times 10^{-8} \text{ N - sec}^2\text{-m) escape-wheel)}
\end{aligned}$$

### Gear Train Driving Escapement

The escapement of the M525 fuze is driven by a clock spring through a step-up gear train with a ratio of 45.98. The timing function of the fuze, which involves a delay of between 2 to 4 seconds, is accomplished once the spring driven input gear has rotated through  $310^\circ$ . This corresponds to a 45.98 times greater escape-wheel rotation. Since the motion becomes stabilized after one cycle of the pallet (corresponding to approximately  $40^\circ$  of escape-wheel rotation), one obtains an excellent idea of the total time by computing the response time for  $310^\circ$  of escapement rotation and multiplying this result by the aforementioned gear ratio (see the section on results for standard configuration).

### Standard Torque Used in the Simulation

Measurements on actual fuzes showed that the initial torque on the escape-wheels varied between .0177 ( $2.000 \times 10^{-3}$  m-N) and .031 in-lb ( $3.503 \times 10^{-3}$  m-N). Since the angle of rotation of the input gear is small, the decrease in torque during the rotation is also relatively small. Therefore, a constant torque was assumed in the simulation. Its standard value was chosen to be .0177 in-lb ( $2.000 \times 10^{-3}$  m-N).

### Other Dimensions Associated With Standard Configuration

For purposes of control in the computer program the following other dimensions are of interest.

The maximum absolute value attainable for the dimension  $g$  for the given escapement is computed according to equation (H-4) of appendix H:

$$g_{MAX} = -.05467 \text{ inches } (-.1389 \text{ cm})$$

The associated values of the escape-wheel angle  $\varphi_M$  are obtained with the use of equation H-10. For top action

$$\varphi_M = 132.487^\circ$$

Because of this value, initial coupled motion is started at  $135^\circ$ . (See the section on the computer program.) For bottom action, this angle becomes:

$$\varphi_M = 187.518^\circ$$

The corresponding values for the pallet angles  $\psi_M$  are found through the use of equation (A.8) appendix A and are computed with  $g = -.05467$  and  $\alpha = 40^\circ$ . For top action,

$$\psi_M = 39.491^\circ$$

and for bottom action,

$$\psi_M = 320.396^\circ$$

These values serve as valuable checks on the computer output.

The escape-wheel angles  $\varphi_O$  corresponding to  $g = 0$ , i.e. the position when the pallet pin leaves the tooth in coupled motion, are obtained according to equation (H-12). For top action,

$$\varphi_O = 146.328^\circ$$

Because of this angle, decisions concerning indexing, the free motion and impact tests are based on whether the angle  $\varphi$  is smaller or larger than  $150^\circ$ . (See the section on the description of the computer program.) For bottom action, this angle becomes

$$\varphi_O = 206.512^\circ$$

The corresponding pallet angles are

$$\psi_O = 60.138^\circ \text{ for top action, and}$$

$$\psi_O = 299.869^\circ \text{ for bottom action, respectively.}$$



Finally, it is important to know the center distance between pallet and escape-wheel for which disengagement will occur. According to equation (G.14)

$$a_{dis} = .208 \text{ inches } (.528 \text{ cm})$$

## RESULTS FOR STANDARD CONFIGURATION

Appendix I shows computer output for the first, second and eighth cycles of a run for the standard configuration with a coefficient of friction,  $\mu = .3$ , and a coefficient of restitution,  $\epsilon = .25$  (run no. 46). Table 1 summarizes the results of the first two and one half cycles. In appendix I, a cycle is defined as the interval between first contacts on top. In tables 1 and 3 the interval is between the last contacts on top.) As discussed earlier, top motion in the coupled mode initiates the program. In the subsequent first bottom action, the first impact is followed by free motion while the second impact leads to coupled motion by virtue of the cut-off criterion. Starting with the second top contact, both top and bottom action consists of two impacts followed by free motion. The subsequent third impact produces little rebound of the pallet pin and thus is the beginning of coupled motion which lasts until the pallet pin leaves the tooth.

The various impacts cause reversals in escape-wheel motion. In the actual mechanism, this backward rotation is limited by the possibility of the pin making contact with the backface of the next escape-wheel tooth. The program does not provide for the presence of this condition and any contact of this type makes itself known only if during or after the first impact, the escape-wheel angle  $\phi < 132.487^\circ$  for top action or  $\phi < 187.518^\circ$  for bottom action. If such a reversal of the escape-wheel takes place during coupled motion,  $g$  will be less than  $-.05467 \text{ in. } (-.1284 \text{ cm})$ . (See the section on other dimensions of the standard configuration for discussion of the above values.)

Inspection of table 1 shows that this condition first occurs in cycle no. 3 for top contact, i.e.  $\phi = 132.480^\circ$ . Table 2 gives the values of the maximum reversal angles for the first eight cycles. While these reversals of the escape-wheel angle never reach critical values for bottom action, they exceed critical values a number of times for top action. (The geometry lends itself more for this condition with respect to top action.)

The fact that the absolute value of  $g_{MAX}$  will be exceeded in certain configurations will be accepted or more dissipative values for  $\mu$  and  $\epsilon$  will have to be used<sup>5</sup>. The discussion in the section on the influence of parameter changes in the total fuze time will show that a slight increase of the center distance decreases the absolute value of  $g$  at maximum reversal to well below  $g_{MAX}$ . This correlates with the results for  $\mu = .3$  and  $\epsilon = 0$  given below.

Table 1 shows that the stability of motion is essentially established during the first cycle. The time interval per cycle, now counted between the instants when the pallet pin leaves the top tooth, is shown to be .00774 and .00773 seconds. Subsequent intervals (not shown here) are .00773, .00775, .00785, .00784, and .00773 seconds. The total time of the fuze may be obtained with the help of the time at PHITOT  $\approx 310^\circ$ . Appendix I shows that  $t(310.362^\circ) = .06058$  seconds. Thus, the total fuze delay time becomes  $.06058 \times 45.98 = 2.79$  seconds. (See the section on the example mechanism.) This result is well within the fuze requirement of between 2 to 4 seconds.

Appendix J gives portions of the computer output when the standard configuration was run with  $\epsilon = 0$ , while  $\mu = .3$  was kept (run no. 70). Table 3 summarizes the events of the first  $3\frac{1}{2}$  cycles and table 4 lists the maximum reversal values of the escape-wheel for eight cycles.

As expected, the fully inelastic coefficient of restitution causes the initial impacts to be followed by coupled motion. Now,  $g < g_{MAX}$  at all times. (Again, the reversals are smaller for bottom action.) As in the first program above, the motion stabilizes immediately with cycle intervals of .00725, .00730 and .00725 seconds. Subsequent intervals, not shown here, are .00726, .00729 and .00726 seconds. The total fuze delay time is computed with  $t(\text{PHITOT} = 310.600^\circ) = .05699$  seconds (see appendix J). This results in 2.62 seconds.

<sup>5</sup>Since no high speed motion-pictures of the M525 are available, it is not known whether contact with the backside of the escape-wheel tooth is ever made.

Table 1. Summary of events in the first 2 cycles for standard configuration  
with  $\mu = .3$  and  $c = .25$  (Program No. 46)

Type of action	Escape-wheel angle $\varphi$ (deg)	Time (sec)	Time interval (sec)	Total escape-wheel angle (deg)
Top: start of coupled motion	135.000	0.00000		0.000
start of free motion (end of tooth)	146.491	0.00340 <sup>1</sup>		11.491
Bottom: impact followed by free motion	194.179	0.00382		19.179
maximum return motion (free)				
continued free motion	192.911	0.00402		17.911
impact followed by coupled motion (cut-off criterion: $\ V_P\  - \ V_S\  < 2$ )	193.366	0.00415		18.366
maximum return motion (coupled)	193.281	0.00425		18.281
start of free motion (end of tooth)	206.844	0.00645		31.844
Top: impact followed by free motion	135.522	0.00688		40.522
maximum return motion (free)				
continued free motion	133.361	0.00714		38.361
impact followed by free motion	133.435	0.00720		38.435
maximum return motion	133.214	0.00724		38.214
impact followed by coupled motion (cut-off criterion)	133.214	0.00724		38.214
maximum return motion (coupled)	133.540	0.00753		37.540
start of free motion (end of tooth)	146.514	0.01114 <sup>2</sup>	0.00774 <sup>3</sup>	51.514
Bottom: impact followed by free motion	193.802	0.01154		58.802
maximum return motion (free)				
continued free motion	192.321	0.01176		57.321
impact followed by free motion	192.803	0.01189		57.803
maximum return motion (free)				
continued free motion	192.749	0.01193		57.749
impact followed by coupled motion (cut-off criterion)	192.790	0.01197		57.790
start of free motion (end of tooth)	206.768	0.01417		71.768
Top: impact followed by free motion	135.519	0.01460		80.519
maximum return motion (free)				
continued free motion	132.397	0.01487		78.297
impact followed by free motion	133.394	0.01493		78.394
maximum return motion (free)	133.165	0.01497		78.165
impact followed by coupled motion (cut-off criterion)	133.165	0.01497		78.165
maximum return motion (coupled)	132.480	0.01526		77.480
start of free motion (end of tooth)	146.496	0.01887 <sup>4</sup>	0.00773 <sup>5</sup>	91.496

<sup>1</sup>Start of first cycle

<sup>2</sup>End of first cycle, start of second cycle

<sup>3</sup>Time interval for first cycle

<sup>4</sup>End of second cycle

<sup>5</sup>Time interval for second cycle

Table 2. Maximum reversal angles and associated values of g for  
standard configuration with  $\mu = .3$  and  $\varepsilon = .25$   
(Program No. 46)

Cycle No.	Top action		Bottom action	
	Maximum reversal angle, $\varphi$ ( $\varphi_M = 132.487^\circ$ )	g (in.) ( $g_M = -.05467$ )	Maximum reversal angle, $\varphi$ ( $\varphi_M = 187.518^\circ$ )	$g^1$ (in.) ( $g_M = -.05467$ )
1			192.910	
2	132.540	-.0547 (-.1389 cm)	192.321	
3	132.480	-.0549 (-.1394 cm)	192.303	
4	132.312	-.0555 (-.1410 cm)	192.320	
5	132.305	-.0555 (-.1410 cm)	192.485	
6	132.094	-.0562 (-.1427 cm)	191.837	
7	131.593	-.0580 (-.1473 cm)	192.078	
8	132.634	-.0543 (-.1379 cm)	192.315	

<sup>1</sup>Not applicable. Occurs during free motion.

Table 3. Summary of events in the first 3½ cycles for standard configuration  
with  $\mu = .3$  and  $\varepsilon = 0$  (Program No. 70)

	Type of action	Escape- wheel angle $\varphi$ (deg)	Time		Total escape- wheel angle (deg)
			(sec)	interval (sec)	
Top:	start of coupled motion	135.000	0.00000		0.000
	start of free motion	146.491	0.00340 <sup>1</sup>		11.491
Bottom:	impact followed by coupled motion	194.179	0.00382		19.179
	maximum return motion (coupled)	193.776	0.00404		18.776
	start of free motion	206.789	0.00622		31.789
Top:	impact followed by coupled motion	135.416	0.00665		40.416
	maximum return motion (coupled)	133.957	0.00711		38.957
	start of free motion	146.743	0.01065 <sup>2</sup>	0.00725 <sup>3</sup>	51.743
Bottom:	impact followed by coupled motion	193.636	0.01104		58.636
	maximum return motion (coupled)	193.083	0.01129		58.083
	start of free motion	207.171	0.01354		72.171
Top:	impact followed by coupled motion	135.168	0.01395		80.168
	maximum return motion (coupled)	133.504	0.01443		78.504
	start of free motion	146.383	0.01795 <sup>4</sup>	0.00730 <sup>5</sup>	91.383
Bottom:	impact followed by coupled motion	194.198	0.01837		99.198
	maximum return motion (coupled)	193.698	0.01861		98.698
	start of free motion	206.601	0.02077		111.601
Top:	impact followed by coupled motion	135.600	0.02121		120.600
	maximum return motion	134.171	0.02167		119.171
	start of free motion	146.856	0.02521 <sup>6</sup>	0.00725 <sup>7</sup>	131.856

<sup>1</sup> Start of first cycle

<sup>2</sup> End of first cycle, start of second cycle

<sup>3</sup> Time interval for first cycle

<sup>4</sup> End of second cycle, start of third cycle

<sup>5</sup> Time interval for second cycle

<sup>6</sup> End of third cycle

<sup>7</sup> Time interval for third cycle

Table 4. Maximum reversal angles and associated values of g for  
standard configuration with  $\mu = .3$  and  $\varepsilon = 0$   
(Program No. 70)

Cycle No.	Top action		Bottom action	
	Maximum reversal angle, $\varphi$ ( $\varphi_M = 132.487^\circ$ )	g (in.) ( $g_M = -.05467$ )	Maximum reversal angle, $\varphi$ ( $\varphi_M = 187.518^\circ$ )	$g^1$ (in.) ( $g_M = -.05467$ )
1			193.776	-.0401 (-.1019 cm)
2	133.957	-.0495 (-.1257 cm)	193.083	-.0418 (-.1062 cm)
3	133.504	-.0512 (-.1300 cm)	193.698	-.0403 (-.1024 cm)
4	134.171	-.0487 (-.1237 cm)	192.883	-.0423 (-.1074 cm)
5	133.466	-.0513 (-.1303 cm)	193.659	-.0404 (-.1026 cm)
6	134.170	-.0487 (-.1237 cm)	192.883	-.0423 (-.1074 cm)
7	133.466	-.0513 (-.1303 cm)	193.659	-.0404 (-.1026 cm)
8	134.170	-.0487 (-.1237 cm)	192.884	-.0423 (-.1074 cm)

## INFLUENCE OF VARIOUS PARAMETER CHANGES ON THE TOTAL FUZE TIME

The following reports on the results of numerous computer runs in which a single input or geometric parameter was varied in order to determine its influence on the total fuze time. In all cases, the individual changes were made with respect to the standard configuration in the section on the example mechanism, with  $\mu = .3$  and  $\epsilon = .25$ .

### Influence of Escape-Wheel Torque

Figure 8 shows the influence of the escape-wheel torque on the fuze time. One may compare these timing results with those obtained from the well-known empirical expression:

$$t_2 = t_1 \sqrt{\frac{T_1}{T_2}}$$

If  $t_1$  and  $T_1$  represent fuze time and torque, respectively, as associated with the standard configuration, one obtains from the above:

$$\text{For } T_2 = .75 T_1, \quad t_2 = 2.79 \sqrt{\frac{1}{1.25}} = 3.22 \text{ seconds}$$

$$\text{For } T_2 = 1.25 T_1, \quad t_2 = 2.79 \sqrt{\frac{1}{1.25}} = 2.49 \text{ seconds}$$

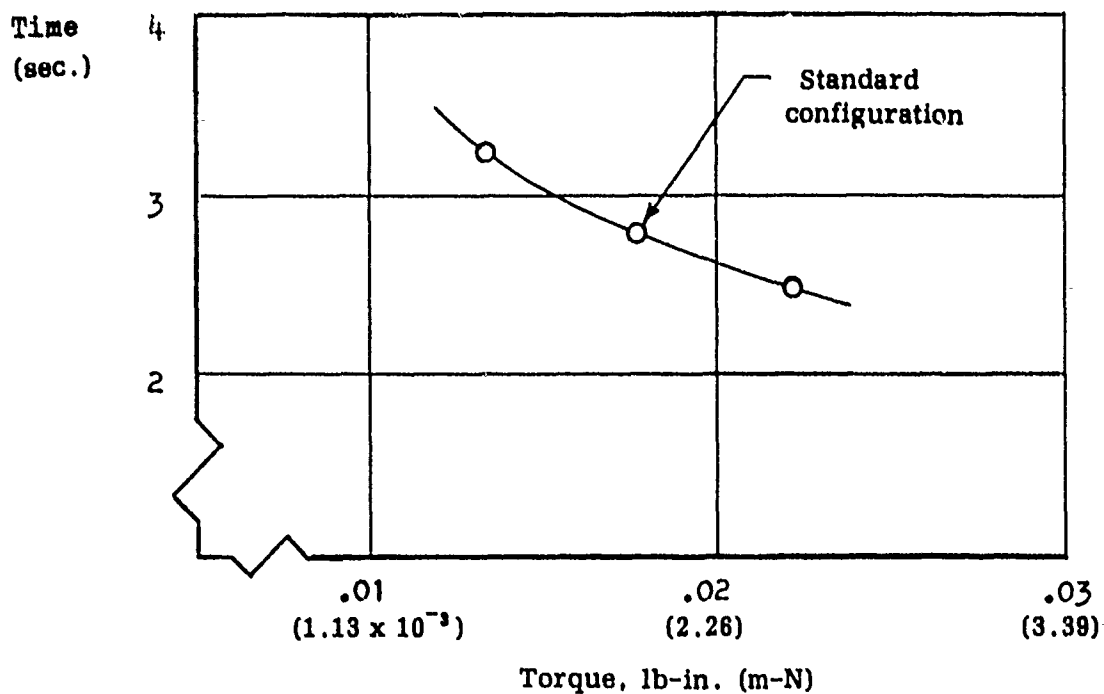
The results of the simulation (runs 47 and 48 of table of figure 8) show excellent agreement with the above. The empirical relationship has been confirmed time and again by experiment.

### Influence of Pallet Moment of Inertia

Figure 9 shows that the total fuze delay time increases with an increase of the pallet moment of inertia. The ratio of any two fuze periods is approximately proportional to the ratio of the square roots of the associated pallet inertias. These results are confirmed by the experiments of Anderson and Redmond (ref. 7).

### Influence of Pallet Escape-Wheel Center Distance

Figure 10 indicates, for the range explored, that the fuze time increases as the center distance  $a$  is increased. For a total increase of .007 inches (.018 cm), the time increase is approximately 7%. This result is



Run no.	Torque (lb-in.)	Total Fuze Time (sec.)
48	.0133 (75% of St.) ( $1.503 \times 10^{-3}$ m-N)	3.23
46	.0177 (St.) ( $2.000 \times 10^{-3}$ m-N)	2.79
47	.0221 (125% of St.) ( $2.497 \times 10^{-3}$ m-N)	2.50

Figure 8. Influence of escape-wheel torque on fuze delay time



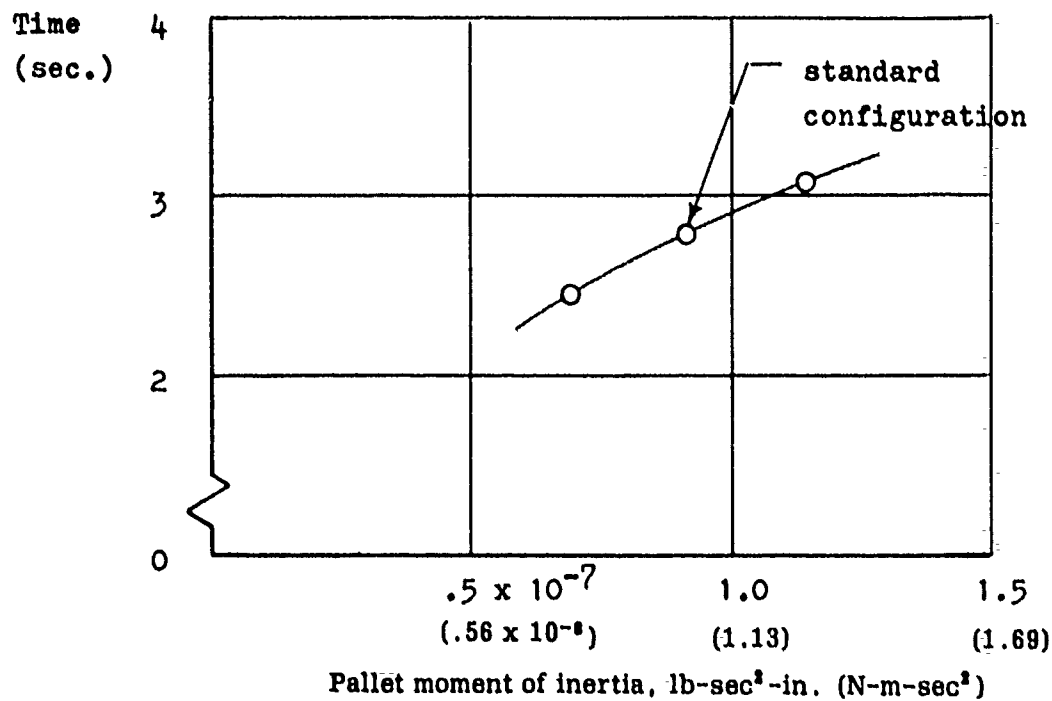
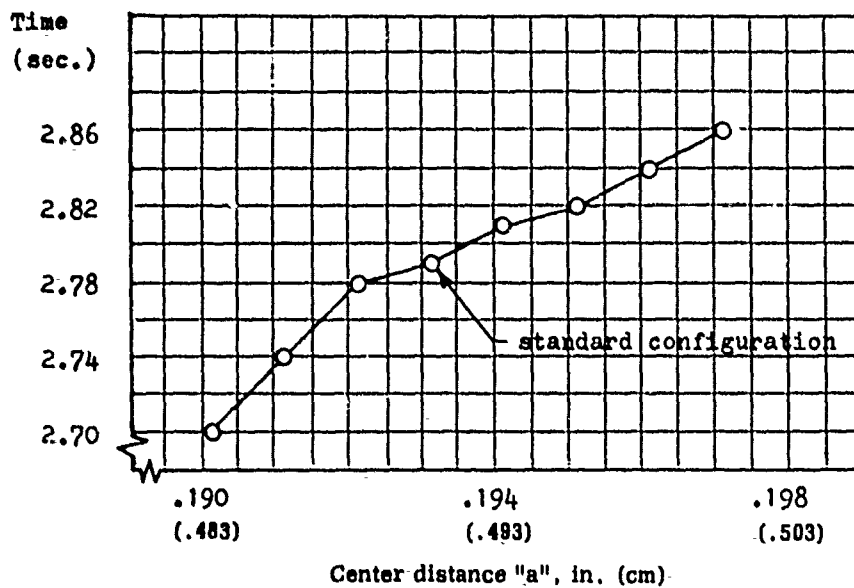


Figure 9. Influence of pallet moment of inertia on fuze delay time



Run no.	Center distance "a" (in.)	Total fuze time (sec.)
55	.1901	2.70
54	.1911 (.4854 cm)	2.74
53	.1921 (.4879 cm)	2.78
46	.1931 (std. conf.) (.4905 cm)	2.79
49	.1941 (.4930 cm)	2.81
50	.1951 (.4956 cm)	2.82
51	.1961 (.4981 cm)	2.84
52	.1971 (.5006 cm)	2.86

Figure 10. Influence of pallet escape-wheel center distance on fuze delay time

generally confirmed by the experimentation of Anderson and Redmond (ref. 7), where it is shown that an increase of time is effected as the center distance is increased from a dimension somewhat below nominal.

#### **Influence of Pallet Radius**

Figure 11 shows a continuous and quite dramatic decrease in fuze period as the pallet radius  $c$  is increased by .008 inches (.020 cm). It is believed that this effect is similar to that observed in connection with a decrease in center distance  $a$ , i.e. an increase in pallet radius represents an effective decrease of center distance. The experimentation performed in reference 7 gives good correlation with this result of the simulation.

#### **Influence of Coefficient of Friction**

Figure 12 indicates that the fuze time increases as the coefficient of friction, associated with coupled motion, is increased. One would expect that an increase of energy dissipation will slow the mechanism.

#### **Influence of Coefficient of Restitution**

According to figure 13, the fuze time increases considerably as the coefficient of restitution is varied from completely inelastic to partially elastic; i.e. from zero to .5. When  $\epsilon = 0$  (see description of run no. 70 in the section on results for standard configuration), coupled motion follows immediately after impact. In run no. 75 (which is not reproduced in this report), where  $\epsilon = .5$ , top action consists of four impacts, three of which are followed by free motion while the fourth is followed by coupled motion. Bottom action shows two impacts with the last one followed by coupled motion. Each of the impacts is followed by considerable escape-wheel reversal. These multiple impacts and associated motion reversals seem to account for the observed increase in fuze time.

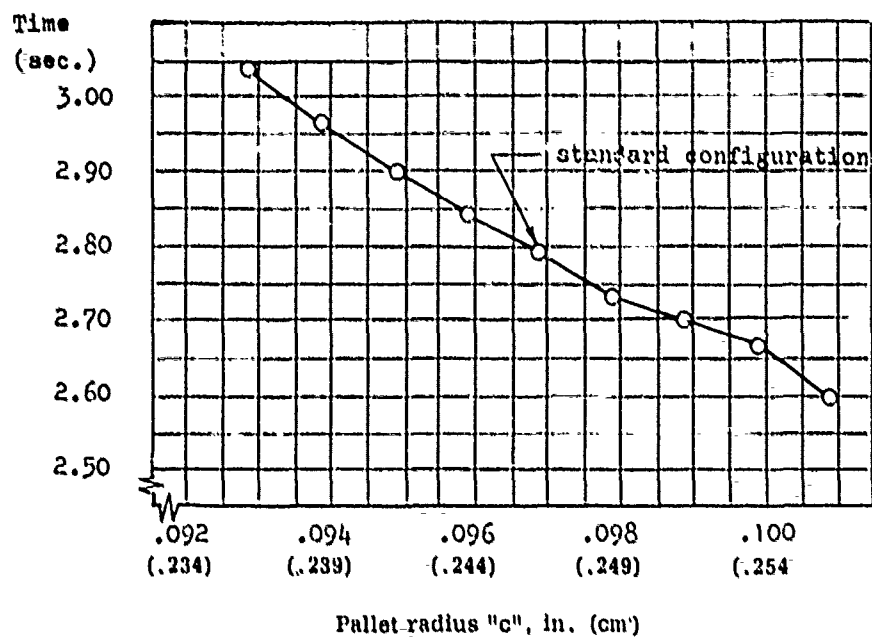
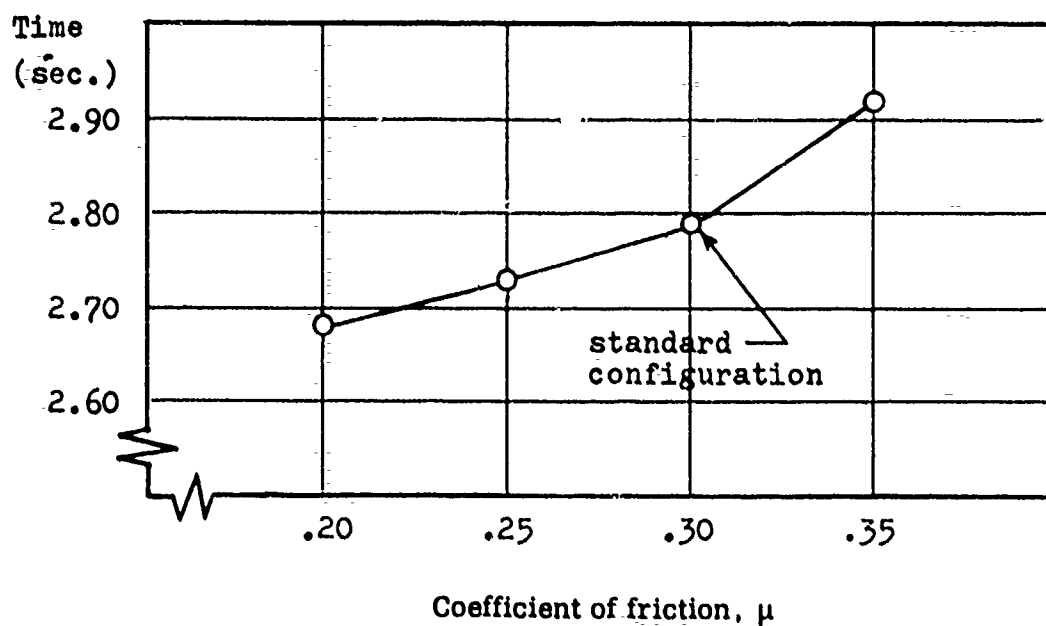
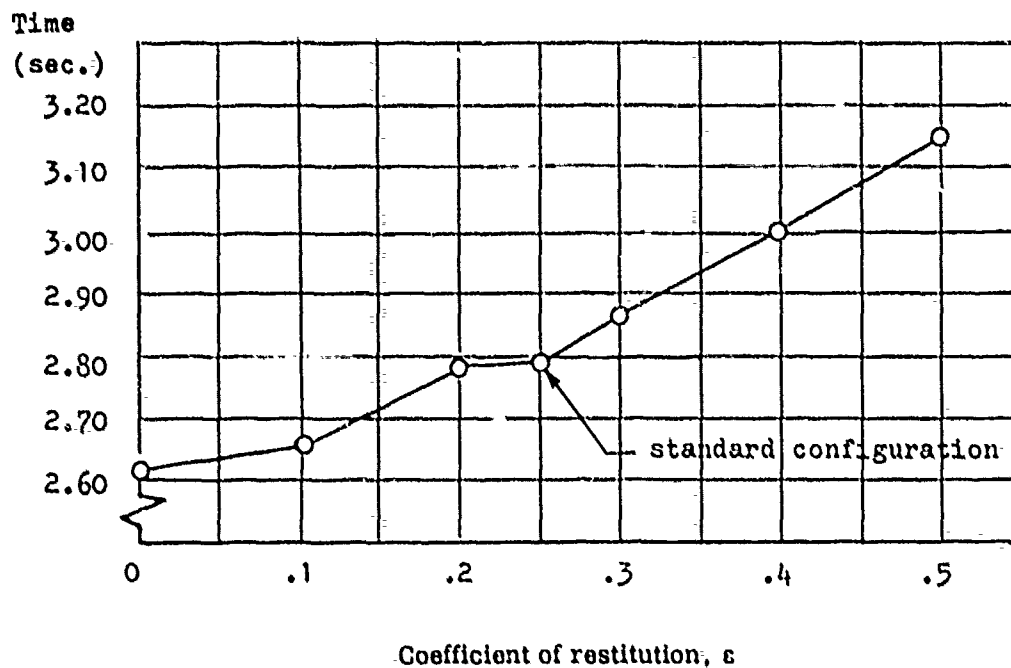


Figure 11. Influence of pallet radius on fuze delay time



Run no.	Coefficient of friction, $\mu$	Total fuze time (sec.)
68	.20	2.68
67	.25	2.73
46	.30 (std. conf.)	2.79
69	.35	2.92

Figure 12. Influence of coefficient of friction of coupled motion on fuze delay time



Run no.	Coefficient of restitution, $\epsilon$	Total fuze time (sec.)
75	.5	3.15
74	.4	3.01
73	.3	2.87
46	.25 (std. conf.)	2.79
72	.2	2.78
71	.1	2.66
70	0.0	2.62

Figure 13. Influence of coefficient of restitution on fuze delay time

## DISCUSSION AND RECOMMENDATIONS FOR CONTINUED WORK

There is no doubt that the goal of a workable computer simulation of the pin pallet runaway escapement has been attained. This is mainly due to the fact that every effort was made to keep the program and its controls as simple as possible.

As a consequence of this, there is presently no built-in sensing mechanism that indicates whether the pallet pin makes contact with the backside of an adjacent tooth during free motion. While this abnormality did not occur for the M525 mechanism, there is no assurance that it will never occur.

Secondly, there is the unresolved problem of the somewhat excessive escape-wheel reversal for the standard configuration unless fairly unrealistic values are used for the coefficients of friction and restitution. (Recall the discussion in the section on the results for the standard configuration.) Table 5 shows the extent to which this escape-wheel reversal depends on the center distance between the pallet and escape-wheel pivots.

Clearly, the reversal increases with a decrease in center distance and decreases as the center distance is enlarged. Note, that for  $a = .1941$  inches (.4930 cm), which is .001 in (.0025 cm) above nominal,  $|g| < |g_{MAX}|$ . Note further, that the disengagement center distance of .208 inches (.528 cm) (see end of the section on the example mechanism) is much larger than the values which have been explored in table 5.

Excessive escape-wheel reversal may be indicative of the fact that the simple impact formulation is not sufficiently descriptive, as shown by Anderson and Redmond (ref. 7) or that the escapement only operates in the expected manner when the center distance is somewhat enlarged from nominal.

To resolve this problem, high speed motion pictures must be taken in order to be able to observe the actual motion. Following this, certain modifications of the impact model may have to be made.

Even if the question of the motion reversal cannot be fully resolved, the present simulation is sufficiently descriptive to undertake the following extensions:

1. Adaptation of the pin pallet runaway escapement simulation to a centrifugally driven mechanism, such as the M577 safe separation device (SSD) .<sup>6</sup>

2. Adaptation of the pin pallet simulation to a spring-driven timing mechanism .

3. Modification of the present model to accommodate the simulation of a plate pallet (verge) type runaway escapement.

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<sup>6</sup>Successful simulations, incorporating the present escapement model, of both the M577 SSD and the M125A1 booster have been recently completed. The results will be given in a future report.



Table 5. Escape-wheel reversal as a function of center distance a

Center distance, a* (in.)	Value of g at maximum reversal during top action (in.)	Program number
.1901 (.4829 cm)	-.0662 (-.1681 cm)	55
.1911 (.4854 cm)	-.0635 (-.1613 cm)	54
.1921 (.4879 cm)	-.0600 (-.1524 cm)	53
.1931 (std. conf.) (.4905 cm)	-.0580 (-.1473 cm)	46
.1941 (.4930 cm)	-.0536 (-.1361 cm)	49
.1951 (.4956 cm)	-.0520 (-.1321 cm)	50
.1961 (.4981 cm)	-.0471 (-.1196 cm)	51
.1971 (.5006 cm)	-.0441 (-.1120 cm)	52

\*Dimension a is variable, otherwise dimensions are standard configuration with  $\mu = .3$ ,  $\varepsilon = .25$  and  $g_{MAX} = -.05467$  in. (-.13886 cm).

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## APPENDIX A

### KINEMATICS OF COUPLED MOTION

Figure A1 shows the kinematic relationship of the escape-wheel and the pallet during coupled motion.

#### UNIT VECTORS

The unit vectors  $\bar{n}_t$  and  $\bar{n}_n$  are along and perpendicular to the contact surface of the escape-wheel tooth in the indicated directions, respectively. Thus,

$$\bar{n}_t = \cos(\varphi - \alpha) \bar{i} + \sin(\varphi - \alpha) \bar{j} \quad (A1)$$

$$\bar{n}_n = -\sin(\varphi - \alpha) \bar{i} + \cos(\varphi - \alpha) \bar{j} \quad (A2)$$

In addition, the unit vectors  $\bar{n}_b$ , for the escape-wheel, and  $\bar{n}_c$ , for the line connecting the pallet pivot and the center of the pallet pin, are introduced:

$$\bar{n}_b = \cos \varphi \bar{i} + \sin \varphi \bar{j} \quad (A3)$$

$$\bar{n}_c = \cos \psi \bar{i} + \sin \psi \bar{j} \quad (A4)$$

#### INPUT - OUTPUT RELATIONSHIP

The mechanism loop equation is used to determine the pallet angle  $\psi$  and the pallet pin location  $g$  with respect to the tip of the escape-wheel as functions of the escape-wheel angle  $\varphi$  and the applicable mechanism constants, i.e.

$$\begin{aligned} 0 = & b(\cos \varphi \bar{i} + \sin \varphi \bar{j}) + g[\cos(\varphi - \alpha) \bar{i} + \sin(\varphi - \alpha) \bar{j}] \\ & + r[-\sin(\varphi - \alpha) \bar{i} + \cos(\varphi - \alpha) \bar{j}] - c(\cos \psi \bar{i} + \sin \psi \bar{j}) \\ & + a \bar{i} \end{aligned} \quad (A5)$$

The above is rewritten in component form:

$$b \cos \varphi + g \cos(\varphi - \alpha) - r \sin(\varphi - \alpha) - c \cos \psi + a = 0 \quad (A6)$$

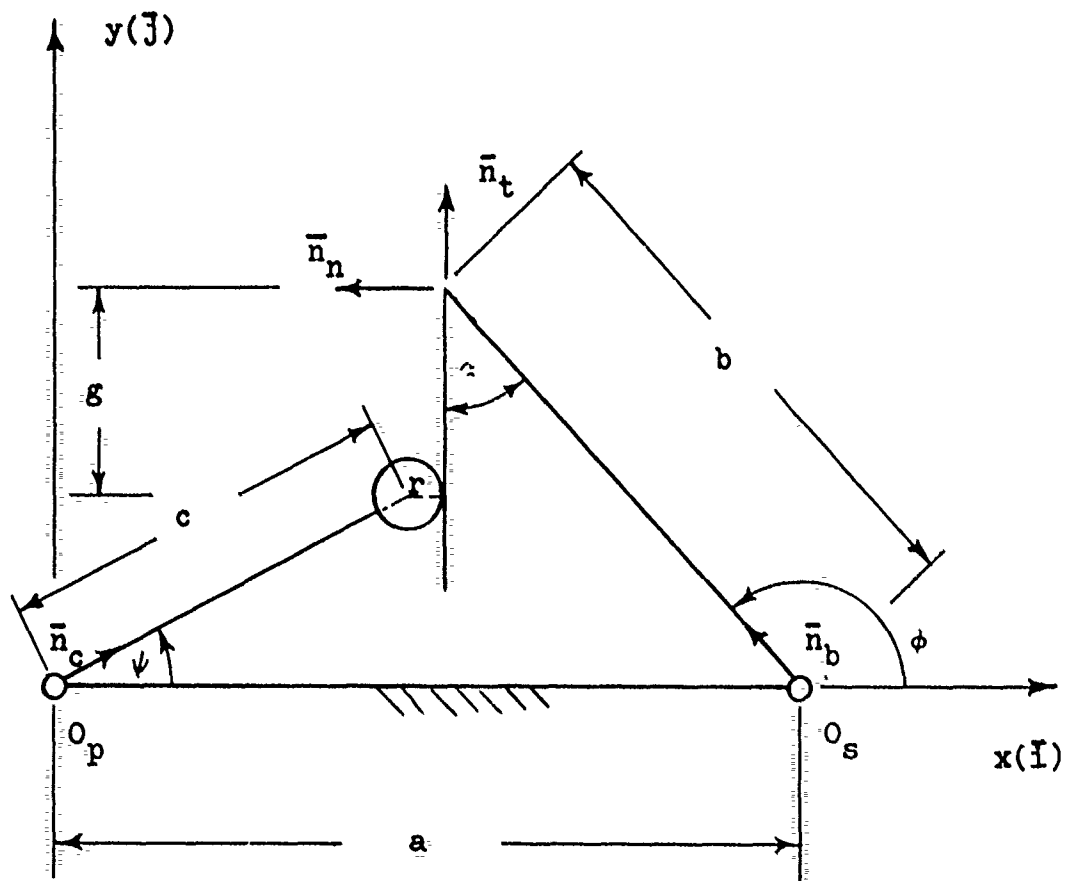


Figure A1. Coupled motion kinematics

$$b \sin \varphi + g \sin(\varphi - \alpha) + r \cos(\varphi - \alpha) - c \sin \psi = 0 \quad (A7)$$

The angle  $\psi$  is obtained from (A7):

$$\sin \psi = \frac{1}{c} [b \sin \varphi + g \sin(\varphi - \alpha) + r \cos(\varphi - \alpha)] \quad (A8)$$

and

$$\cos \psi = \frac{1}{c} \sqrt{c^2 - [b \sin \varphi + g \sin(\varphi - \alpha) + r \cos(\varphi - \alpha)]^2} \quad (A9)$$

Substitution of equation (A9) into equation (A6) and subsequent squaring of both sides of the resulting expression leads to:

$$\begin{aligned} [b \cos \varphi + g \cos(\varphi - \alpha) - r \sin(\varphi - \alpha) + a]^2 \\ = c^2 - [b \sin \varphi + g \sin(\varphi - \alpha) + r \cos(\varphi - \alpha)]^2 \end{aligned} \quad (A10)$$

Rearrangement gives:

$$\begin{aligned} g^2 + g[2b \cos \alpha + 2a \cos(\varphi - \alpha)] \\ + [a^2 + b^2 + r^2 - c^2 + 2br \sin \alpha + 2ab \cos \varphi - 2ar \sin(\varphi - \alpha)] \\ = 0 \end{aligned} \quad (A11)$$

Finally, solution of equation (A11) leads to:

$$g = \frac{-H \pm \sqrt{H^2 - 4K}}{2} \quad (A12)$$

where

$$H = 2[b \cos \alpha + a \cos(\varphi - \alpha)] \quad (A13)$$

$$K = a^2 + b^2 + r^2 - c^2 + 2br \sin \alpha + 2ab \cos \varphi - 2ar \sin(\varphi - \alpha) \quad (A14)$$

The correct value of  $g$ , as obtained from equation (A12), must have the smaller absolute magnitude.

## OUTPUT VELOCITIES

Implicit differentiation of equation (A11) furnishes the velocity  $\dot{g}$  of the instantaneous contact point on the pallet with respect to the coincident point on the escape-wheel during coupled motion:

$$\dot{g} = \frac{a P}{S} \dot{\varphi} \quad (A15)$$

where

$$P = b \sin \varphi + g \sin(\varphi - \alpha) + r \cos(\varphi - \alpha) \quad (A16)$$

$$S = g + b \cos \alpha + a \cos(\varphi - \alpha) \quad (A17)$$

Differentiation of equation (A8) leads to the pallet angular velocity during coupled motion:

$$\dot{\psi} = \frac{Q \dot{\varphi} + \dot{g} \sin(\varphi - \alpha)}{(c) \cos \psi} \quad (A18)$$

where

$$Q = b \cos \varphi + g \cos(\varphi - \alpha) - r \sin(\varphi - \alpha) \quad (A19)$$

## OUTPUT ACCELERATIONS

Differentiation of equation (A15) results in an expression for the relative acceleration of the contact point on the pallet with respect to that on the escape-wheel:

$$\ddot{g} = \frac{\ddot{\varphi} P a + \dot{\varphi}^2 Q a + 2 \dot{\varphi} \dot{g} a \sin(\varphi - \alpha) - \dot{g}^2}{S} \quad (A20)$$

Further, differentiation of equation (A18) furnishes an expression for the angular acceleration of the pallet during coupled motion:

$$\begin{aligned} \ddot{\psi} = & \frac{\ddot{\varphi} Q - \dot{\varphi}^2 P + 2 \dot{g} \dot{\varphi} \cos(\varphi - \alpha) + \ddot{g} \sin(\varphi - \alpha)}{c \cos \psi} \\ & + \dot{\psi}^2 \tan \psi \end{aligned} \quad (A21)$$

## APPENDIX B

### DIFFERENTIAL EQUATION OF COUPLED MOTION

Figure B-1 shows free body diagrams of the pallet and escape-wheel, as they are found during coupled motion. The torque  $T$  acts on the escape-wheel. The forces between the escape-wheel and the pallet are represented by the normal forces  $\pm \bar{P}_n$  in the direction of  $\bar{n}_n$  and the friction forces  $\pm (\mu \bar{P}_n)$  in the direction of  $\bar{n}_t$ . The sign of the friction forces must be such that when the contact point  $K$  on the pallet pin moves in the direction of the positive velocity  $\dot{g}$  with respect to the coincident point  $L$  on the escape-wheel, the friction force on the pallet pin must act in the negative direction of  $\dot{g}$ . (Note that  $\dot{g}$ , as given by equation (A15) in appendix A, has the same direction as the relative velocity  $\bar{V}_{K/L}$ .)

The frictional resistance at the pivots  $O_p$  and  $O_s$  is neglected, since the pivot radii are commonly held very small  $\bar{r}_p$  causing the friction moments to become insignificant.

The differential equations of rotation will first be written separately for the pallet and the escape-wheel. Since the output angle  $\psi$  is a function of the input angle  $\phi$  throughout coupled motion, both expressions may be combined by way of the common force magnitudes.

Equation of Motion for the Pallet

$$\bar{D}_1 \times \bar{P}_n \bar{n}_n + \bar{C}_1 \times (-\mu \bar{P}_n \frac{\dot{g}}{|\dot{g}|}) \bar{n}_t = I_p \ddot{\psi} \bar{k} \quad (B1)$$

Equation of Motion for the Escape-Wheel

$$\bar{A}_1 \times (-\bar{P}_n) \bar{n}_n + \bar{B}_1 \times (\mu \bar{P}_n \frac{\dot{g}}{|\dot{g}|}) \bar{n}_t + T \bar{k} = I_s \ddot{\phi} \bar{k} \quad (B2)$$

The moment arms  $\bar{A}_1$ ,  $\bar{B}_1$ ,  $\bar{C}_1$ , and  $\bar{D}_1$  are given by equations (C6), (C7), (C4), and (C5), respectively.  $I_p$  and  $I_s$  represent the moments of inertia of the pallet and the escape-wheel with respect to their pivots.

Appropriate vector operations on equations (B1) and (B2) furnish the following scalar expressions:



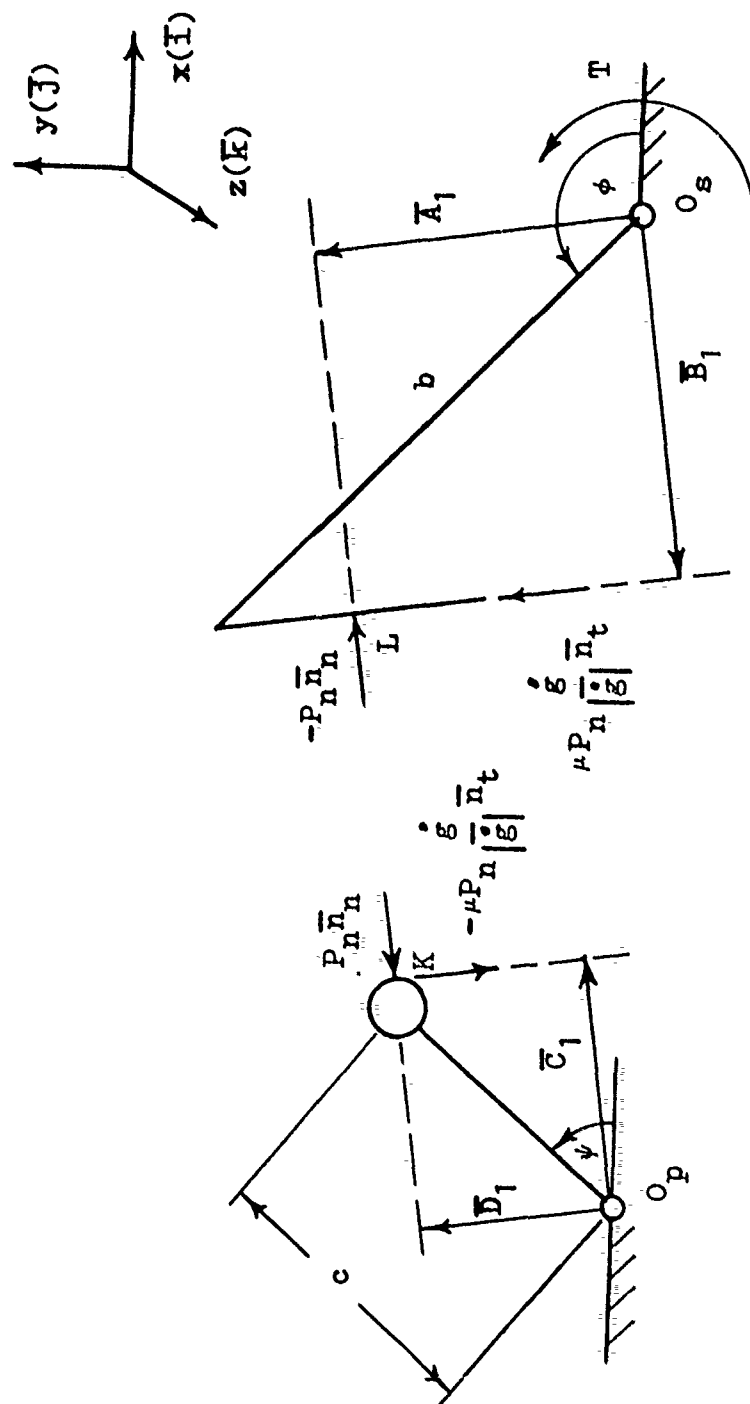


Figure B1. Free body diagram for coupled motion

$$P_n (D_1 - C_1 \mu \frac{\dot{g}}{|\dot{g}|}) = I_p \ddot{\psi} \quad (B3)$$

$$\text{and} \quad -P_n (A_1 + B_1 \mu \frac{\dot{g}}{|\dot{g}|}) + T = I_s \ddot{\phi} \quad (B4)$$

When the above expressions are equated in terms of  $\bar{P}_n$ , one obtains:

$$\frac{I_p (A_1 + \mu B_1 \frac{\dot{g}}{|\dot{g}|})}{(D_1 - \mu C_1 \frac{\dot{g}}{|\dot{g}|})} \ddot{\psi} + I_s \ddot{\phi} = T \quad (B5)$$

The angular acceleration  $\ddot{\psi}$  is now expressed in terms of  $\ddot{\phi}$  and  $\dot{\phi}$  with the help of equation (A21) of appendix A. Equations (A15), (A18), and (A20) are utilized to replace  $\dot{g}$ ,  $\psi$  and  $\ddot{g}$ , respectively. After considerable simplification, one obtains the following expression for  $\ddot{\psi}$ :

$$\ddot{\psi} = U \ddot{\phi} + V \dot{\phi}^2 \quad (B6)$$

where

$$U = \frac{Q + \frac{aP}{S} \sin(\varphi - \alpha)}{(c) \cos \psi} \quad (B7)$$

and

$$\begin{aligned} V = \frac{1}{ccos \varphi} & \left[ \frac{2aP}{S} \cos(\varphi - \alpha) - P + \frac{2a^2P}{S^2} \sin^2(\varphi - \alpha) \right. \\ & \left. + \frac{aQ}{S} \sin(\varphi - \alpha) - \frac{a^2P^2}{S^3} \sin(\varphi - \alpha) \right] \\ & + \frac{\tan \psi}{c^2 \cos^2 \psi} \left[ Q + \frac{Pa}{S} \sin(\varphi - \alpha) \right]^2 \quad (B8) \end{aligned}$$

Equation (B6) is now substituted into equation (B5). This results in:

$$\left[ \frac{I_p U \left( \frac{A_1 + \mu B_1 \frac{\dot{g}}{|g|}}{D_1 - \mu C_1 \frac{\dot{g}}{|g|}} \right) + I_s}{\frac{p}{E_1} + \frac{s}{F_1}} \right] \ddot{\phi} + \frac{I_p V \left( \frac{A_1 + \mu B_1 \frac{\dot{g}}{|g|}}{D_1 - \mu C_1 \frac{\dot{g}}{|g|}} \right)}{\frac{p}{E_1} + \frac{s}{F_1}} (\dot{\phi})^2 = T \quad (B9)$$

For computational purposes, equation (B9) is rewritten in the following form:

$$\ddot{\phi} + W\dot{\phi}^2 = Y \quad (B10)$$

where

$$W = \frac{\frac{I_p V}{E_1}}{\frac{p}{E_1} + \frac{s}{F_1}} \quad (B11)$$

$$Y = \frac{\frac{T}{F_1}}{\frac{p}{E_1} + \frac{s}{F_1}} \quad (B12)$$

and

$$E_1 = D_1 - \mu C_1 \frac{\dot{g}}{|g|} \quad (B13)$$

$$F_1 = A_1 + \mu B_1 \frac{\dot{g}}{|g|} \quad (B14)$$

## APPENDIX C

### MOMENT ARMS

#### DETERMINATION OF MOMENT ARMS $\bar{C}_1$ AND $\bar{D}_1$

Figure C-1 suggests the following loop equation for the determination of the vectors  $\bar{C}_1$  and  $\bar{D}_1$ :

$$c\bar{n}_c - r\bar{n}_n - D_1\bar{n}_n + C_1\bar{n}_n = 0 \quad (C1)$$

When the components in the  $\bar{n}_t$  and  $\bar{n}_n$  directions are separated, one obtains:

$$c\cos\psi + r\sin(\varphi - \alpha) + D_1\cos(\varphi - \alpha) - C_1\sin(\varphi - \alpha) = 0 \quad (C2)$$

and

$$c\sin\psi - r\cos(\varphi - \alpha) + D_1\sin(\varphi - \alpha) + C_1\cos(\varphi - \alpha) = 0 \quad (C3)$$

Simultaneous solution of the above expressions leads to the following vectorial expressions:

$$\bar{C}_1 = - [r + c\sin(\varphi - \alpha - \psi)]\bar{n}_n \quad (C4)$$

and

$$\bar{D}_1 = c\cos(\varphi - \alpha - \psi)\bar{n}_t \quad (C5)$$

#### DETERMINATION OF MOMENT ARMS $\bar{A}_1$ AND $\bar{B}_1$

Inspection of figure C-1 leads to the following expressions for the vectors  $\bar{A}_1$  and  $\bar{B}_1$ :

$$\bar{A}_1 = (b\cos\alpha + g)\bar{n}_t \quad (C6)$$

(Note that  $g$  is negative during contact.)

Further,

$$\bar{B}_1 = (b\sin\alpha)\bar{n}_n \quad (C7)$$



## APPENDIX D

### CONTACT SENSING EXPRESSIONS

When the mechanism is in free motion, i.e.  $\varphi$  and  $\psi$  are independent of each other, it is necessary to know the distances  $f$  and  $g'$ , in figure D-1, to determine the relative positions. The quantity  $f$ , which indicates the distance of the pallet pin from the escape-wheel face, vanishes at the instant of impending impact. When contact between the pallet and the escape-wheel becomes impossible, i.e. the pin has left the tooth,  $g' \geq 0$ .

By inspection of figure D-1, the loop equation for free motion is given by:

$$b\bar{n}_b + g'\bar{n}_t + (r + f)\bar{n}_n - c\bar{n}_c + a\bar{i} = 0 \quad (D1)$$

(Note that  $\varphi$  and  $\psi$  are independent variables and are assumed to be known.)

In component form, the above becomes:

$$b\cos\varphi + g'\cos(\varphi - \alpha) - r\sin(\varphi - \alpha) - f\sin(\varphi - \alpha) - c\cos\psi + a = 0 \quad (D2)$$

$$b\sin\varphi + g'\sin(\varphi - \alpha) + r\cos(\varphi - \alpha) + f\cos(\varphi - \alpha) - c\sin\psi = 0 \quad (D3)$$

Multiply equation (D2) by  $\sin(\varphi - \alpha)$

$$\begin{aligned} & b\cos\varphi\sin(\varphi - \alpha) + g'\sin(\varphi - \alpha)\cos(\varphi - \alpha) - r\sin^2(\varphi - \alpha) \\ & - f\sin^2(\varphi - \alpha) - c\cos\psi\sin(\varphi - \alpha) + a\sin(\varphi - \alpha) \\ & = 0 \end{aligned} \quad (D4)$$

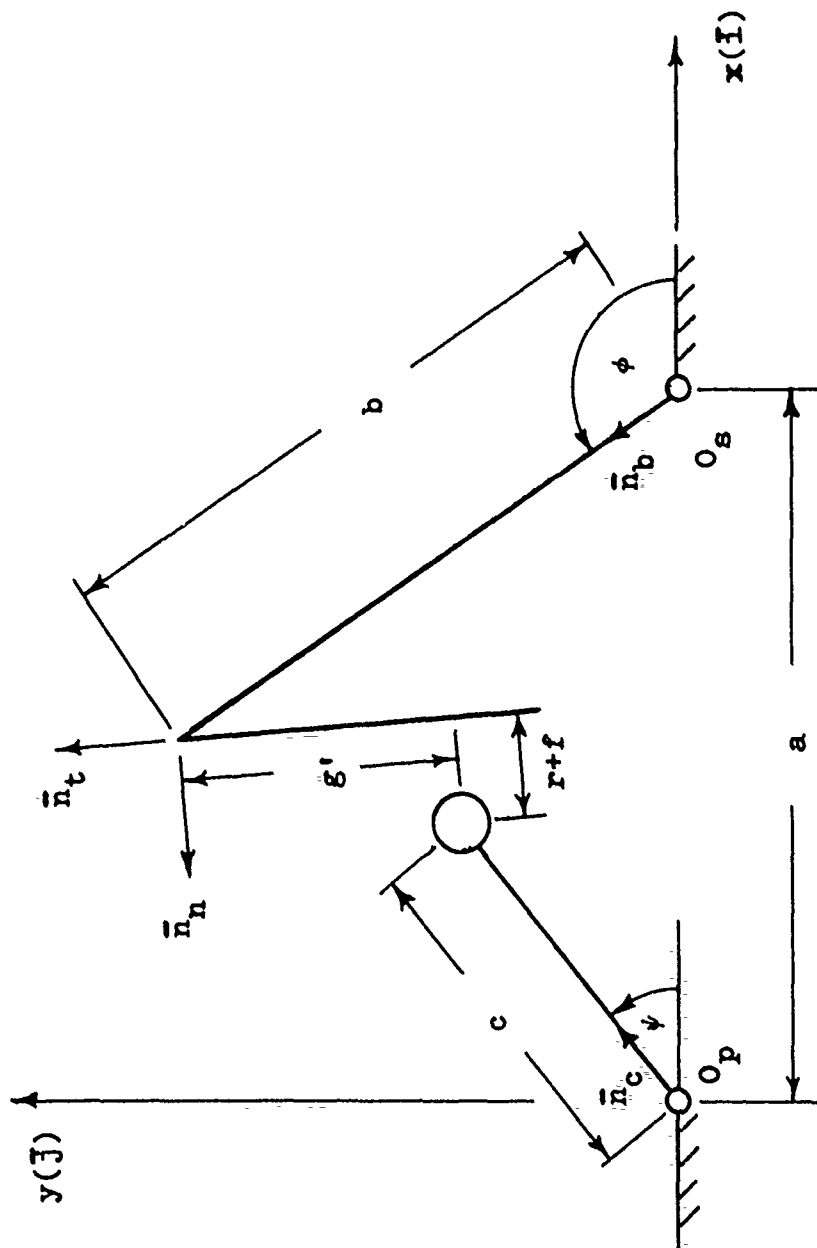


Figure D1. Contact sensing quantities

Further, multiply equation (D3) by  $\cos(\varphi - \alpha)$

$$\begin{aligned} & b\sin\varphi\cos(\varphi - \alpha) + g'\sin(\varphi - \alpha)\cos(\varphi - \alpha) + r\cos^2(\varphi - \alpha) \\ & + f\cos^2(\varphi - \alpha) - c\sin\psi\cos(\varphi - \alpha) \\ & = 0 \end{aligned} \quad (D5)$$

Subtract equation (D4) from equation (D5)

$$\begin{aligned} & b\sin[\varphi - (\varphi - \alpha)] + r + f + c\sin[(\varphi - \alpha) - \psi] - a\sin(\varphi - \alpha) \\ & = 0 \end{aligned} \quad (D6)$$

This furnishes

$$f = a\sin(\varphi - \alpha) - b\sin\alpha - c\sin[(\varphi - \alpha) - \psi] - r \quad (D7)$$

Multiply (D2) by  $\cos(\varphi - \alpha)$

$$\begin{aligned} & b\cos\varphi\cos(\varphi - \alpha) + g'\cos^2(\varphi - \alpha) - r\sin(\varphi - \alpha)\cos(\varphi - \alpha) \\ & - f\sin(\varphi - \alpha)\cos(\varphi - \alpha) - c\cos\psi\cos(\varphi - \alpha) \\ & + a\cos(\varphi - \alpha) \\ & = 0 \end{aligned} \quad (D8)$$

Multiply (D3) by  $\sin(\varphi - \alpha)$

$$\begin{aligned} & b\sin\varphi\sin(\varphi - \alpha) + g'\sin^2(\varphi - \alpha) + r\sin(\varphi - \alpha)\cos(\varphi - \alpha) \\ & + f\sin(\varphi - \alpha)\cos(\varphi - \alpha) - c\sin\psi\sin(\varphi - \alpha) \\ & = 0 \end{aligned} \quad (D9)$$

Finally, add (D8) and (D9)

$$\begin{aligned} & b\cos[\varphi - (\varphi - \alpha)] + g' - c\cos[\psi - (\varphi - \alpha)] + a\cos(\varphi - \alpha) \\ & = 0 \end{aligned} \quad (D10)$$

Thus,

$$g' = c\cos[(\varphi - \alpha) - \psi] - b\cos\alpha - a\cos(\varphi - \alpha) \quad (D11)$$



## APPENDIX E

### FREE MOTION EQUATIONS

During the free motion phase of the mechanism, the pallet moves independently of the escape-wheel.

Again, the frictional resistance at the pivots  $O_p$  and  $O_s$  are neglected.

### FREE MOTION OF PALLET

In the absence of all external torques, the differential equation of motion for the pallet is given by:

$$\ddot{\psi} = 0 \quad (E1)$$

With an initial angular velocity  $\dot{\psi}_0$  at the time  $t_0$ , when the free motion starts, the angular velocity of the pallet at any time is:

$$\dot{\psi} = \dot{\psi}_0 \quad (E2)$$

If  $\psi(t_0) = \psi_0$ , further integration gives the angular displacement of the pallet at any time  $t$  to be:

$$\psi = \dot{\psi}_0 (t - t_0) + \psi_0 \quad (E3)$$

The time  $t$  is counted from the start of the motion of the escapement.

### FREE MOTION OF THE ESCAPE-WHEEL

When a constant torque  $T$  acts on the escape-wheel, its differential equation of motion is given by:

$$\ddot{\phi} = \frac{T}{I_s} \quad (E4)$$

and the applicable initial conditions are:

$$\dot{\phi}(t_0) = \dot{\phi}_0 \quad (E5)$$

and

$$\varphi(t_0) = \varphi_0 \quad (E6)$$

Integration of equation (E4) gives the following expression for the angular velocity of the escape-wheel at any time  $t$ :

$$\dot{\varphi} = \frac{T}{I_s} (t - t_0) + \dot{\varphi}_0 \quad (E7)$$

Further integration furnishes the angular displacement:

$$\varphi = \frac{T}{2I_s} (t - t_0)^2 + \dot{\varphi}_0 (t - t_0) + \varphi_0 \quad (E8)$$

## APPENDIX F

### IMPACT EQUATIONS

Before the impact equations can be given, certain velocity expressions associated with the impact points on the pallet and the escape-wheel must be derived. These velocities occur during free motion preceding impact when the angular velocities  $\dot{\phi}$  and  $\dot{\psi}$  are independent of each other.

#### VELOCITIES AT IMPACT POINTS JUST BEFORE IMPACT

Figure F1 shows the velocities of the contact points K and L on the pallet and the escape-wheel, respectively, just before impact. The components in the direction normal to the escape-wheel tooth are:

$$\bar{V}_{pn_i} = \dot{\psi}_i \bar{k} \times D_1 \bar{n}_t \quad \text{for the pallet} \quad (F1)$$

and

$$\bar{V}_{sn_i} = \dot{\phi}_i \bar{k} \times A_1 \bar{n}_t \quad \text{for the escape-wheel,} \quad (F2)$$

where the subscript i stands for the angular velocities prior to the instant of impact.

The components of velocity in the tangential direction are given by:

$$\bar{V}_{pt_i} = \dot{\psi}_i \bar{k} \times C_1 \bar{n}_n \quad (F3)$$

and

$$\bar{V}_{st_i} = \dot{\phi}_i \bar{k} \times B_1 \bar{n}_n \quad (F4)$$

The expressions for the moment arms are obtained from appendix C.

To determine the direction of the tangential impact, the sign of the relative tangential velocity  $\bar{V}_t$  must be known. This velocity is given by (refer to equations (F3) and (F4)):

$$\bar{V}_t = \bar{V}_{pt_i} - \bar{V}_{st_i} = \dot{\psi}_i \bar{k} \times C_1 \bar{n}_n - \dot{\phi}_i \bar{k} \times B_1 \bar{n}_n \quad (F5)$$

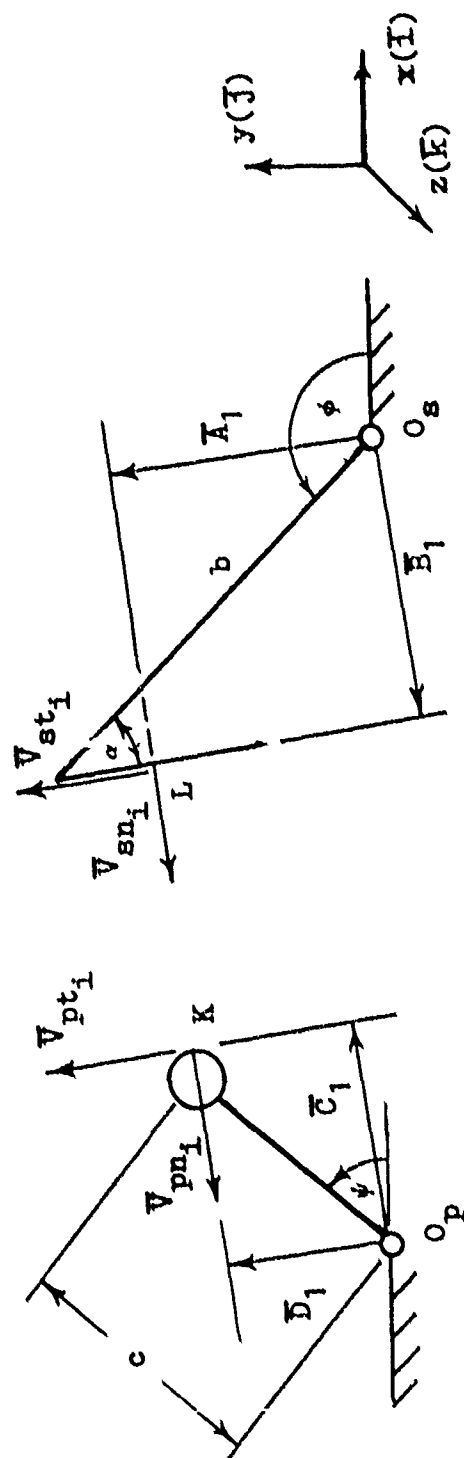


Figure F1. Velocities just before impact

Substituting equations (C4) and (C7) into equation (F5) produces:

$$\bar{V}_t = (\psi[r + c \sin(\varphi - \alpha - \psi)] + \phi b \sin \alpha) \bar{n}_t \quad (F6)$$

### IMPACTS ON PALLET AND ESCAPE-WHEEL

The impact simulation is based on the classical angular impulse-momentum model shown in figure F-2 for the pallet and the escape-wheel.

$\bar{P}_n$  represents the normal impulse between the components. Further, a frictional impulse  $\mu \bar{P}_n$ , which is tangential to the contact surface and has the direction of the velocity  $\bar{V}_t$  (see equation (F6)), is assumed because of the angular displacements during impact.

The angular impulse  $T_t$  on the escape-wheel, which is due to the torque  $T$  and has the duration  $t$  of the impact phenomenon, is disregarded since it is felt that its magnitude is small when compared to that of the other terms involved. The angular impulse on the pallet then becomes:

$$\bar{J}_p = \bar{D}_1 \times \bar{P}_n \bar{n}_n + \bar{C}_1 \times -\mu \bar{P}_n \frac{V_t}{|\bar{V}_t|} \bar{n}_t \quad (F7)$$

After the cross product has been executed, the following equation is obtained:

$$\bar{J}_p = \bar{P}_n (D_1 - \mu C_1 \frac{V_t}{|\bar{V}_t|}) \bar{k} \quad (F8)$$

Similarly, the angular impulse on the escape-wheel reduces to:

$$\bar{J}_s = \bar{A}_1 \times (-\bar{P}_n) \bar{n}_n + \bar{B}_1 \times \mu \bar{P}_n \frac{V_t}{|\bar{V}_t|} \bar{n}_t \quad (F9)$$

This becomes

$$\bar{J}_s = -\bar{P}_n (A_1 + \mu B_1 \frac{V_t}{|\bar{V}_t|}) \bar{k} \quad (F10)$$

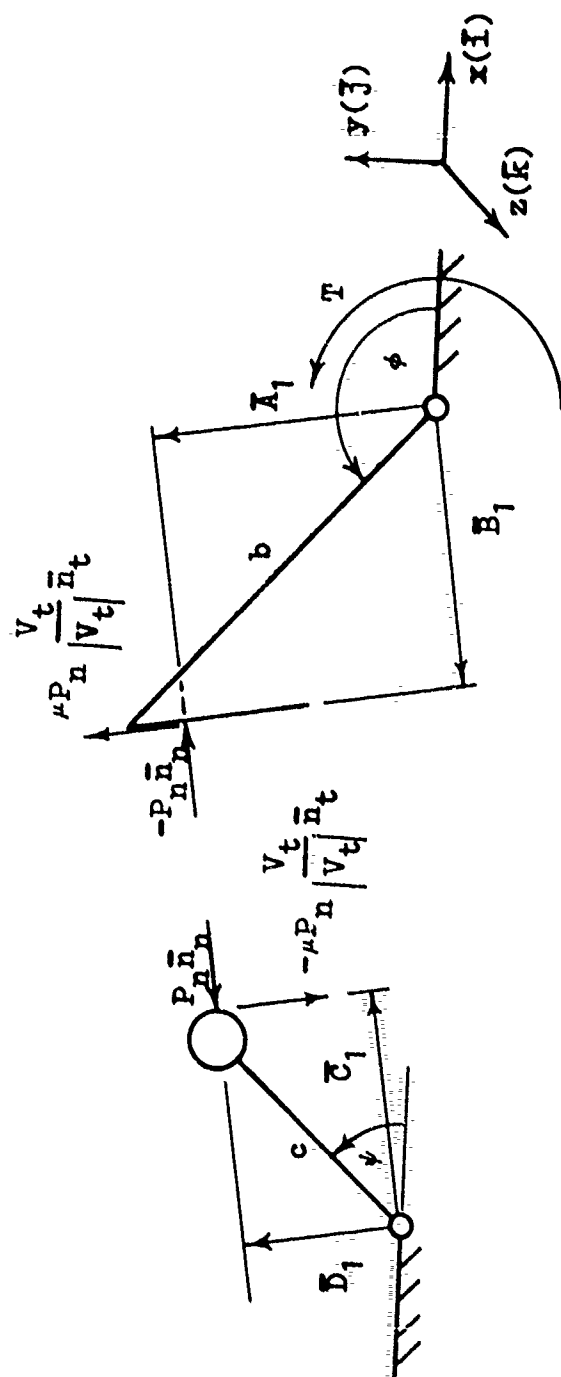


Figure F2. Free body diagram of impact

Equations (F8) and (F10) are now substituted into the following angular momentum equations:

$$I_p (\psi_f - \psi_i) = \bar{J}_p \quad (F11)$$

and

$$I_s (\phi_f - \phi_i) = \bar{J}_s \quad (F12)$$

The subscript f indicates the angular velocities after impact. Substitution of the scalar portions of equations (F8) and (F10) into equations (F11) and (F12), respectively, as well as the subsequent simultaneous elimination of  $P_n$  from both of the resulting expressions, leads to:

$$I_p F_2 \psi_f + I_s E_2 \phi_f = I_p F_2 \psi_i + I_s E_2 \phi_i \quad (F13)$$

where

$$E_2 = D_1 - \mu C_1 \frac{V_t}{|V_t|} \quad (F14)$$

and

$$F_2 = A_1 + \mu B_1 \frac{V_t}{|V_t|} \quad (F15)$$

To solve for the angular velocities after impact, it is now necessary to make use of the concept of the coefficient of restitution. This coefficient is adapted to the present situation in the following manner:

$$\epsilon = - \frac{V_{pn_f} - V_{sn_f}}{V_{pn_i} - V_{sn_i}} \quad (F16)$$

Using equations (F1) and (F2) and letting

$$\bar{V}_{pn_f} = \psi_f \bar{k} \times D_1 \bar{n}_t \quad \text{for the pallet} \quad (F17)$$

$$\bar{V}_{sn_f} = \dot{\phi}_f \bar{k} \times A_1 \bar{n}_t \quad \text{for the escape-wheel} \quad (F18)$$

where  $\dot{\phi}_f$  and  $\dot{\psi}_f$  are the respective angular velocities of the pallet and the escape-wheel after impact, produces

$$\varepsilon = - \frac{(\dot{\psi}_f D_1 - \dot{\phi}_f A_1)}{(\dot{\psi}_i D_1 - \dot{\phi}_i A_1)} \quad (F19)$$

Simultaneous solution of equations (F13) and (F19) furnishes the desired angular velocities after impact.

Thus,

$$\dot{\psi}_f = \frac{\dot{\phi}_f A_1 - \varepsilon (\dot{\psi}_i D_1 - \dot{\phi}_i A_1)}{D_1} \quad (F20)$$

and

$$\dot{\phi}_f = \frac{I_p F_2 \dot{\psi}_i + I_s E_2 \dot{\phi}_i + \frac{I_p F_2 \varepsilon}{D_1} (\dot{\psi}_i D_1 - \dot{\phi}_i A_1)}{\frac{I_p F_2 A_1}{D_1} + I_s E_2} \quad (F21)$$

#### GENERAL EXPRESSIONS FOR THE NORMAL VELOCITIES AT THE IMPACT POINTS

The normal velocities at the impact points of the pallet and the escape-wheel are also used in the logic of the computer program. If  $\dot{\phi}$  and  $\dot{\psi}$  represent the angular velocities of the escape-wheel and the pallet just before or after impact, expressions are derived for these velocities using (F1), (F2), (C5), and (C6):

For the pallet

$$V_p = \dot{\psi} c \cos(\varphi - \alpha - \psi) \quad (F22)$$

For the escape wheel

$$V_s = \dot{\phi} (b \cos \alpha + g) \quad (F23)$$

(Note the simplification of the notation.)



**APPENDIX G**  
**COMPUTER PROGRAM**



```

55 IF (G.LT.0.1) GO TO 200
   PHID=PHI(1)/Z
   IF (PHID.LE.150.1) GO TO 150
   GO TO 151
150 PHI(1)=PHI(1)*DELTA*Z
   PHIPR = PHI(1)/Z
   PSI=PSI+2.*PI-LAMBDA*Z
   GO TO 200
60
151 PHI(1)=PHI(1)-DELTA*Z*2.
   PHIPR = PHI(1)/Z
   PSI=PSI-2.*PI-LAMBDA*Z
65 C FREE MOTION
   C
   C 200 CALL FREE(TIME,PHI(1),PHI(2),PSI,DPSI)
   C
70 C
   C
   C
   PHID=PHI(1)/Z
   H=2.*(B*COS(ALPHR)+A*COS(PHI(1)-ALPHR))
   K=A**2+8.*R**2-C**2+2.*B*R*SIN(ALPHR)+2.*A*B
   I=COS(PHI(1))-2.*A*R*SIN(PHI(1)-ALPHR)
   GONE=(-H-SORT(H**2-4.*K))/2.
   GTWO=(-H-SORT(H**2-4.*K))/2.
   IF (ABS(GONE).LT.ABS(GTWO)) GO TO 204
   G=GTWO
80 GO TO 205
   204 G=GONE
   205 PHID=PHI(1)/Z
   GP=C*COS(PHI(1)-ALPHR-PSI)-B*COS(ALPHR)-A*COS(PHI(1)
1-ALPHR)
   IF (GP.LT.0.1) GO TO 250
   IF (PHID.LE.150.1) GO TO 210
   GO TO 215
210 PHI(1)=PHI(1)+DELTA*Z
   PHIPR = PHI(1)/Z
   PSI = PSI + 2.*PI - LAMBDA*Z
   GO TO 200
215 PHI(1)=PHI(1)-DELTA*Z*2.
   PHIPR = PHI(1)/Z
   PSI = PSI - 2.*PI - LAMBDA*Z
   GO TO 200
250 IF (PHID.LE.150.1) GO TO 9
   DPSIP=DPSI
95
100 C COMPUTATION OF VELOCITIES VP AND VS FOR BOTTOM FREE MOTION TESTS
   C
   C
   AONE=B*COS(ALPHR)*G
   DONE=C*COS(PHI(1)-ALPHR-PSI)
   VP=DONE*DPSI
   VS=AONE*PHI(2)
   WRITE(6,9002)VP,VS
105 9002 FORMAT('0VP=',F8.3X,'VS=',F8.3)

```

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PROGRAM ESCHT 73/74 OPT=1

## C BOTTOM FREE MOTION TESTS

```
110 IF (PHI(2).GE.0..AND.DPSI.GE.0.)GO TO 300
    IF (PHI(2).GE.0..AND.DPSI.LE.0..AND.ABS(VP).GT.ABS(VS))GO TO 200
    IF (PHI(2).GE.0..AND.DPSI.LE.0..AND.ABS(VP).LT.ABS(VS))GO TO 300
    IF (PHI(2).GE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
    IF (PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).GT.ABS(VS))GO TO 300
    IF (PHI(2).LE.0..AND.DPSI.GE.0..AND.ABS(VP).GT.ABS(VS))GO TO 300
    IF (PHI(2).LE.0..AND.DPSI.GE.0..AND.ABS(VP).LT.ABS(VS))GO TO 200
    IF (PHI(2).LE.0..AND.DPSI.GE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
    IF (PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).GT.ABS(VS))GO TO 300
```

## C COMPUTATION OF VELOCITIES VP AND VS FOR TOP FREE MOTION TESTS

```
120 9 AONE=B*COS(ALPHR)*G
    DONE=C*COS(PHI(1)-ALPHR-PSI)
    VP=DONE*DPSI
    VS=AONE*PHI(2)
    WRITE(6,9002)VP,VS
```

## C TOP FREE MOTION TESTS

```
130 IF (PHI(2).GE.0..AND.DPSI.GE.0..AND.ABS(VP).GT.ABS(VS))GO TO 200
    IF (PHI(2).GE.0..AND.DPSI.GE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
    IF (PHI(2).GE.0..AND.DPSI.GE.0..AND.ABS(VP).LT.ABS(VS))GO TO 300
    IF (PHI(2).LE.0..AND.DPSI.GE.0..AND.ABS(VP).GT.ABS(VS))GO TO 300
    IF (PHI(2).LE.0..AND.DPSI.GE.0..AND.ABS(VP).LT.ABS(VS))GO TO 200
    IF (PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).LT.ABS(VS))GO TO 200
    IF (PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).GT.ABS(VS))GO TO 300
    IF (PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
    IF (PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99
```

## C IMPACT

```
140 300 CALL IMPACT(PHI(1),PHI(2),PSI,DPSI)
    R=2.*(4*COS(ALPHR)+A*COS(PHI(1)-ALPHR))
    K=A*(2.8**2-R**2-C**2)*.8**SIN(ALPHR)-2.*A*B
    L=COS(PHI(1))-2.*A*R*SIN(PHI(1)-ALPHR)
    GONE=(-H*SORT(H**2-4.*K))/2.
```

```
145 GTWO=(-H*SORT(H**2-4.*K))/2.
    IF (ABS(GONE).LT.ABS(GTWO))GO TO 310
    G=GTWO
    GO TO 311
```

```
150 310 G=GONE
    311 DPSI=DPSI
    IF (TIME.GT.0.1)GO TO 9999
```

## C TEST FOR BOTTOM ACTION

```
155 PHI0=PHI(1)/2
    IF (PHI0.LE.150.0)GO TO 12
```

## C COMPUTATION OF VELOCITIES VP AND VS FOR BOTTOM IMPACT TESTS

C

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160 AONE=B\*COS(ALPH)\*G  
 DONE=C\*COS(PHI(1))-ALPHA-PSI  
 VP=DONE\*DPSI  
 VS=AONE\*PHI(2)

165 WRITE(6,9002)VP,VS  
 IF(ABS(ABS(VP)-ABS(VS)).LT. 2.0)GO TO 99

C  
 C BOTTOM IMPACT TESTS  
 C

170 IF(PHI(2).GE.0..AND.DPSI.GE.0.)GO TO 99  
 IF(PHI(2).GE.0..AND.DPSI.LE.0..AND.ARS(VP).GT.ABS(VS))GO TO 200  
 IF(PHI(2).GE.0..AND.DPSI.LE.0..AND.ABS(VP).LT.ABS(VS))GO TO 99  
 IF(PHI(2).GE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99  
 IF(PHI(2).LE.0..AND.DPSI.GT.0..AND.ARS(VP).LT.ABS(VS))GO TO 200  
 IF(PHI(2).LE.0..AND.DPSI.GT.0..AND.ABS(VP).GT.ABS(VS))GO TO 99  
 IF(PHI(2).LE.0..AND.DPSI.GT.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99

C  
 C COMPUTATION OF VELOCITIES VP AND VS FOR TOP IMPACT TESTS  
 C

180 12 AONE=B\*COS(ALPH)\*G  
 DONE=C\*COS(PHI(1))-ALPHA-PSI  
 VP=DONE\*DPSI  
 VS=AONE\*PHI(2)

185 WRITE(6,9002)VP,VS  
 IF(ABS(ABS(VP)-ABS(VS)).LT. 2.0)GO TO 99

C  
 C TOP IMPACT TESTS  
 C

190 IF(PHI(2).GE.0..AND.DPSI.GE.0..AND.ABS(VP).GT.ABS(VS))GO TO 200  
 IF(PHI(2).GE.0..AND.DPSI.GE.0..AND.ABS(VP).LT.ABS(VS))GO TO 99  
 IF(PHI(2).GE.0..AND.DPSI.GE.0..AND.ARS(VP).GT.ABS(VS))GO TO 99  
 IF(PHI(2).GE.0..AND.DPSI.GE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99  
 IF(PHI(2).LE.0..AND.DPSI.GT.0..AND.ARS(VP).LT.ABS(VS))GO TO 200  
 IF(PHI(2).LE.0..AND.DPSI.GT.0..AND.ABS(VP).GT.ABS(VS))GO TO 99  
 IF(PHI(2).LE.0..AND.DPSI.GT.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99

195 IF(PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).LT.ABS(VS))GO TO 200  
 IF(PHI(2).LE.0..AND.DPSI.LE.0..AND.ARS(VP).GT.ABS(VS))GO TO 99  
 IF(PHI(2).LE.0..AND.DPSI.LE.0..AND.ABS(VP).EQ.ABS(VS))GO TO 99

9999 STOP  
 ENO

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```
1 SUBROUTINE FCY(I,PHI,DPHI)
  REAL IP,IS,LAMBDA,K
  COMMON A,B,C,R,ALPHR,PI,TOR,K,COFR,IP,IS,TEREST,LAMBDA,DELTA,
  5 LPHITOT,PHIPR
  DIMENSION PHI(2),DPHI(2),PMI(S)
  H=2.*R*COS(ALPHR)*A*COS(PHI(1)-ALPHR)
  K=A**2.*R**2.*R**2-C**2.*B**2.*SIN(ALPHR)**2.*A*B
  10 COS(IPH(1))-2.*A*R*SIN(PHI(1)-ALPHR)
  GONE=(-H*SORT(H**2-4.*K))/2.
  GTWO=(-H*SORT(H**2-4.*K))/2.
  IF (ABS(GONE).LT.ABS(GTWO))GO TO 10
  G=GTWO
  GO TO 11
  10 G=GONE
  11 P=B*SIN(PHI(1))*G*SIN(PHI(1)-ALPHR)+R*COS(PHI(1)-ALPHR)
  Q=B*COS(PHI(1))*G*COS(PHI(1)-ALPHR)+R*SIN(PHI(1)-ALPHR)
  S=G*B*COS(ALPHR)*A*COS(PHI(1)-ALPHR)
  GDOT=PHI(2)*A*P/S
  PSI=ASIN(P/C)
  20 IF (PSI.LT.0.)GO TO 12
  GO TO 13
  12 PSI=2.*PI-ARS(PSI)
  13 AONE=R*COS(ALPHR)*G
  RONE=R*SIN(ALPHR)
  CONE=R*C*SIN(PHI(1)-ALPHR-PSI)
  DONE=C*COS(PHI(1)-ALPHR-PSI)
  IF (GDOT.EQ.0.)GO TO 20
  GO TO 30
  20 EONE=DONE
  FONE=AONE
  GO TO 40
  30 EONE=DONE-COFR*CONE*GDOT/ARS(GDOT)
  FONE=AONE-COFR*BONE*GDOT/ARS(GDOT)
  40 CONTINUE
  U=(0.*SIN(PHI(1)-ALPHR)+P*A/S)/(C*COS(PSI))
  V=(0.*A*SIN(PHI(1)-ALPHR)/S)**2*TAN(PSI)/(C**2)
  1 COS(PSI)**2*(1./(C*COS(PSI)))*(2.*A*P*COS(PHI(1)-ALPHR)/S
  2-P*2.*A**2*P*(SIN(PHI(1)-ALPHR))**2/S**2*A*Q*SIN(PHI(1)
  3-ALPHR)/S-A**2*P**2*SIN(PHI(1)-ALPHR)/S**3)
  W=(IP*V/EONE)/(IP*U/EONE+IS/FONE)
  Y=(TORK/FONE)/(IP*U/EONE+IS/FONE)
  DPHI(1)=PHI(2)
  DPHI(2)=Y-W*PHI(2)**2
  RETURN
  END
```

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```

1  SUBROUTINE OUTP(I,PHI,OPHI,THLF,NDIM,PRMT)
   REAL IP,IS,LAMBDA,K
   DIMENSION PHI(2),OPHI(2),PRMT(5)
   COMMON A,B,C,R,ALPHR,PI,TORR,COFR,IP,IS,CREST,LAMBDA,DELTA,
1 PHITOT,PHIPR
   COMMON ZEIA/PSI,TIME,G,DPSI,DPSIP
   ZE=180./PI
   IF (T.EQ.0.) DPSIP=0.
   PHID=PHI(1)*Z
10  C COMPUTE PSID
   C
   DELPHI = PHID - PHIPR
   PHITOT = PHITOT + DELPHI
   PHIPR = PHID
   H=2.*(B*COS(ALPHR)+A*COS(PHI(1)-ALPHR))
   X=A*2.*R*2.*C*2.*B*R*SIN(ALPHR)*2.*A*B
   I=COS(PHI(1))-2.*A*B*SIN(PHI(1)-ALPHR)
   GONE=(-H*SQRT(H*2-4.*X))/2.
   GTWO=(-H*SQRT(H*2-4.*X))/2.
   IF (ABS(GONE).LT.ABS(GTWO)) GO TO 1
   G=GTWO
   GO TO 2
15  C
   G=GTWO
   GO TO 2
2  P=B*SIN(PHI(1))*G*SIN(PHI(1)-ALPHR)+C*COS(PHI(1)-ALPHR)
   PSI=ASIN(P/C)
   IF (PSI.LT.0.) PSI=2.*PI-ABS(PSI)
   PSID=PSI*Z
30  C COMPUTE DPSI
   C
   S=G*B*COS(ALPHR)+A*COS(PHI(1)-ALPHR)
   GDOT=PHI(2)*A*P/S
   O=B*COS(PHI(1))*G*COS(PHI(1)-ALPHR)+R*SIN(PHI(1)-ALPHR)
   DPSI=(PHI(2)*O-GDOT*SIN(PHI(1)-ALPHR))/(C*COS(PSI))
35  C
   C TEST FOR CONTINUATION OF COUPLED MOTION
   C
   IF (T.EQ.0.) GO TO 4
   IF (T.EQ.0.) GO TO 4
   IF (NOT.(G.LT.0.).AND.((ABS(DPSI).GT.ABS(DPSIP)).AND.PHI(2)
1.GT.0.).OR.(ABS(DPSI).LT.ABS(DPSIP)).AND.PHI(2).LT.0.)).AND.
2.(NE.0.)) PRMT(5)=1.
   IF (ABS(DPSI).LT.1.) PRMT(5)=0.
45  C WRITE OUTPUT
   C
4  WRITE(6,3) PHID,PHI(2),G,GDOT,PSID,DPSI,PHITOT
3 FORMAT('5X,*,T=,F8.5,3X,*,PHI=,F8.3,3X,*,PHID=,F8.3,3X,
1G=,F9.4,3X,*,GDOT=,F8.3,3X,*,PSID=,F8.3,3X,*,DPSI=,F8.3,
13X,*,PHITOT=,F8.3)
5 DPSIP=DPSI
   TIME=T

```

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SUBROUTINE OUTP

73/74 OPT=1

FTN 4.6+420 12/16/76 15.25.49

PAGE 2

55

RETURN  
END

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1 SUBROUTINE IMPACT(PHI,DPHI,PSI,DPSI)

COMMON A,B,C,R,ALPHR,PT,TORK,COFR,IP,IS,EREST,LAMBDA,DELTA,

PHITOT,PHIPR

REAL IP,IS,LAMRDA,K

5 H=2.\*(B\*COS(ALPHR)+A\*COS(PHI-ALPHR))

K=A\*\*2\*B\*\*2-R\*\*2-C\*\*2-2.\*B\*R\*SIN(ALPHR)+2.\*A\*B\*COS(PHI)-

12.\*A\*R\*SIN(PHI-ALPHR)

GONE=(-H+SQRT(H\*\*2-4.\*K))/2.

GTWO=(-H-SQRT(H\*\*2-4.\*K))/2.

10 IF (ABS(GONE).LT.ABS(GTWO)) GO TO 1

G=GTWO

GO TO 2

1 G=GONE

2 AONE=B\*COS(ALPHR)+G

15 DONE=C\*COS(PHI-ALPHR-PSI)

OPHIIN=DPHI

DPSIIN=DPSI

OPHIF=(IP\*AONE\*DPHIIN+IS\*DONE\*DPHIIN+IP\*AONE\*EREST/DONE\*(DPSIIN

1.\*DONE-OPHIIN\*AONE))/ (IP\*AONE\*\*2/DONE+IS\*DONE)

DPSIF=(OPHIF\*AONE-EREST\*(DPSIIN\*DONE-OPHIIN\*AONE))/DONE

20 PHID=PHI\*150./PI

PSID=PSI\*130./PI

WRITE(6,3)

3 FORMAT(0.5X,'IMPACT\*')

WRITE(6,5)PHID,OPHIF,PSID,DPSIF,PHITOT

25 5 FORMAT(0.19X,'PHI=',F8.3X,'DPHIF=',F8.3X,'PSI=',F8.3X,

1.\*DPSIF=',F8.3X,'PHITOT=',F8.3)

OPHI=DPHIF

DPSI=DPSIF

30 6 RETURN

END

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1 SUBROUTINE FREE(TIME,PHI,DPHI,PSI,DPSI)

REAL IP,IS,LAMBDA,K

COMMON A,B,C,R,ALPHR,PI,TOR,K,COFR,IP,IS,EREST,LAMBDA,DELTA,

PHITOT,PHIPR

T=TIME

Z=PI/LA0.

C RECORD INITIAL VALUES

10 PHIIN=PHI

DPHIIN=DPHI

PSIIN=PSI

DPSIIN=DPSI

WRITE(6,5)

5 FORMAT('0.5X,\*,FREE MOTION\*')

C STARWHEEL MOTION

1 PHI=TORK/(2.\*IS)\*(T-TIME)\*(T-TIME)\*DPHIIN\*(T-TIME)\*PHIIN

PHID=PHI/Z

DELPHI=PHID-PHIPR

PHITOT = PHITOT + DELPHI

PHIPR = PHID

DPHI=TOR/K/IS\*(T-TIME)\*DPHIIN

C PALLET MOTION

PSI = DPSIIN\*(T-TIME) + PSIIN

DPSI = DPSIIN

PSID=PSI/Z

C OUTPUT

WRITE(6,2)T,PHID,DPHI,PSID,DPSI,PHITOT

2 FORMAT('0.5X,\*,F8.3X,\*,PHI=\*,F8.3X,\*,PHDOT=\*,F8.3X,\*,

1\*PSI=\*,F8.3X,\*,PSIDOT=\*,F8.3X,\*,PHITOT =\*,F8.3)

9 IF(T.EO.TIME)GO TO 3

C CHECK FOR CONTINUED FREE MOTION

F=A\*SIN(PHI-ALPHR)-B\*SIN(ALPHR)-C\*SIN(PHI-ALPHR-PSI)-R

GP=C\*COS(PHI-ALPHR-PSI)-B\*COS(ALPHR)-A\*COS(PHI-ALPHR)

IF(F.LE.0.)GO TO 4

C CHECK FOR TOP OR BOTTOM ACTION

IF(GP.LE.0.)GO TO 3

PHID=PHI/Z

IF(PHID.LE.150.)GO TO 6

GO TO 7

6 PHI=PHI+DELTA\*Z

PHIPR = PHI/Z

PSI=PSI+2.\*PI-LAMBDA\*Z

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SUBROUTINE FREE

PSIIN = PSIIN + 2.\*PI\*LAMBDA\*Z

GO TO 3

7 PHI=PHI-DELTA\*Z\*2.

PHIPR = PHI/Z

PSI=PSI-2.\*PI\*LAMBDA\*Z

PHIIN = PHIIN - DELTA\*Z\*2.

PSIIN = PSIIN - 2.\*PI\*LAMBDA\*Z

C INCREMENT TIME

3 Y=T+.00001

C CONTINUE FREE MOTION

GO TO 1

C END OF FREE MOTION

4 TIME=T

RETURN

END

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## APPENDIX H

### SOME GEOMETRIC RELATIONSHIP

#### DETERMINATION OF $g_{MAX}$

Figure H-1 shows the geometrical relationship between the pallet pin of radius  $r$  and the right hand escape-wheel tooth when the quantity  $g$  (equation (A12) in appendix A) reaches its maximum possible absolute value. The following relationship holds between the angles  $\alpha$  and  $\beta$ :

$$\alpha = \beta - \frac{\delta}{2} \quad (H1)$$

where

$$\delta = \frac{360}{N} \quad (H2)$$

and  $N$  stands for the number of teeth on the escape-wheel.

The distance  $\overline{ST}$  of the triangle  $OST$  is determined with the help of the sine law:

$$\overline{ST} = b \frac{\sin(\delta/2)}{\sin(\pi - \beta)} \quad (H3)$$

where  $b$  represents the escape-wheel radius.

Finally,  $g_{MAX}$  is obtained from:

$$g_{MAX} = \overline{ST} - \frac{r}{\tan \beta} \quad (H4)$$

To use  $g_{MAX}$  in connection with expressions derived in appendix A, it must be furnished with a minus sign to conform to the origin of the  $\bar{n}_t - \bar{n}_n$  system.

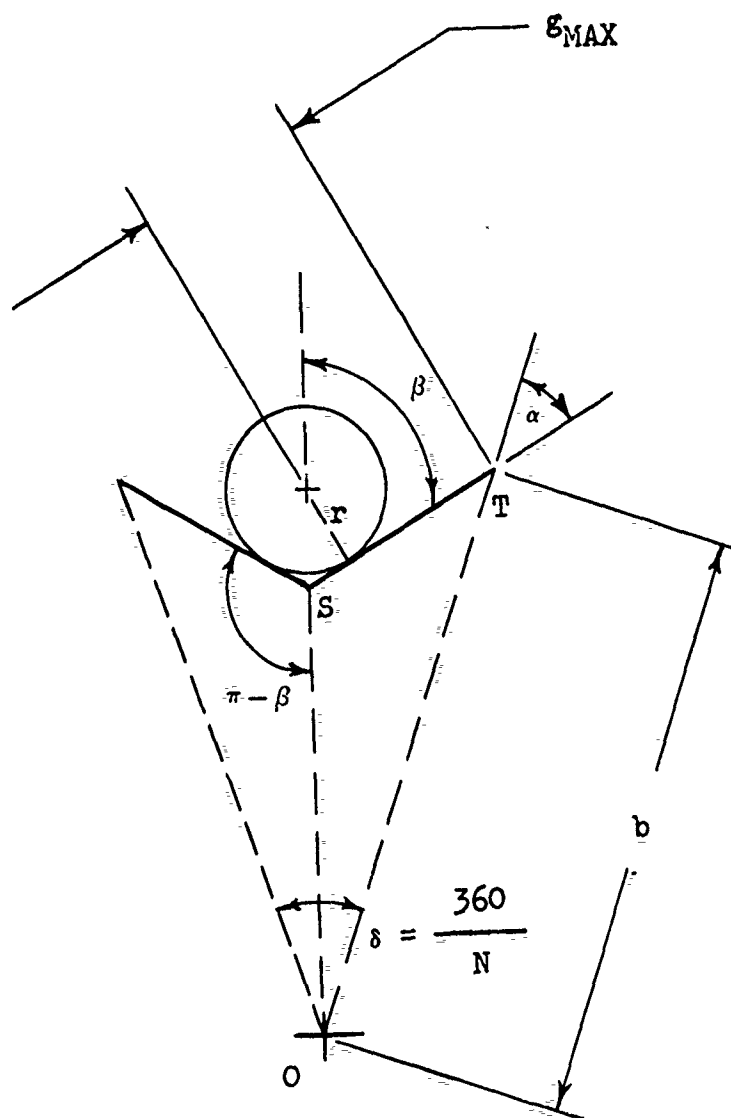


Figure H1. Configuration for  $g_{MAX}$

# DETERMINATION OF ESCAPE-WHEEL ANGLE $\varphi_M$ CORRESPONDING TO $g = g_{MAX}$

The angle  $\varphi = \varphi_M$ , which corresponds to the maximum possible value of  $g = g_{MAX}$ , is obtained with the help of equation (A11) of appendix A:

$$\begin{aligned} g_{MAX}^2 + g_{MAX} [2b \cos \alpha + 2a \cos(\varphi_M - \alpha)] \\ + [a^2 + b^2 + r^2 - c^2 + 2br \sin \alpha + 2ab \cos \varphi_M - 2ar \sin(\varphi_M - \alpha)] \\ = 0 \end{aligned} \quad (H5)$$

After the expansion of the trigonometric terms  $\cos(\varphi_M - \alpha)$  and  $\sin(\varphi_M - \alpha)$ , the following expression results:

$$L \sin \varphi_M + M \cos \varphi_M + N = 0 \quad (H6)$$

where

$$L = 2a(g_{MAX} \sin \alpha - r \cos \alpha)$$

$$M = 2a(g_{MAX} \cos \alpha + b + r \sin \alpha)$$

$$N = g_{MAX}^2 + a^2 + b^2 + r^2 - c^2 + 2b(g_{MAX} \cos \alpha + r \sin \alpha)$$

Equation (H5) may now be rewritten with the help of the following trigonometric identities:

$$\sin \varphi_M = \frac{2 \tan \left( \frac{\varphi_M}{2} \right)}{1 + \tan^2 \left( \frac{\varphi_M}{2} \right)} \quad (H7)$$

$$\cos \varphi_M = \frac{1 - \tan^2 \left( \frac{\varphi_M}{2} \right)}{1 + \tan^2 \left( \frac{\varphi_M}{2} \right)} \quad (H8)$$

This leads to:

$$(N - M) \tan^2 \left( \frac{\varphi_M}{2} \right) + 2L \tan \left( \frac{\varphi_M}{2} \right) + (M + N) = 0 \quad (H9)$$

This expression may now be solved for the angle  $\varphi_M$  using the solution for a quadratic equation. Accordingly,

$$\varphi_M = 2 \tan^{-1} \left[ \frac{-L \pm \sqrt{L^2 - N^2 + M^2}}{N - M} \right] \quad (H10)$$

The two solutions correspond to top and bottom action.

#### DETERMINATION OF ESCAPE-WHEEL ANGLE $\varphi$ CORRESPONDING TO $g = 0$

The angle  $\varphi = \varphi_0$ , which is associated with the instant when the pallet pin leaves the escape-wheel tooth during coupled motion, is obtained from equation (A11) with  $g = 0$ .

An expression similar to equation (H6) results:

$$L_0 \sin \varphi_0 + M_0 \cos \varphi_0 + N_0 = 0 \quad (H11)$$

where

$$L_0 = -2a \cos \alpha$$

$$M_0 = 2a(b + r \sin \alpha)$$

$$N_0 = a^2 + b^2 + r^2 - c^2 + 2br \sin \alpha$$

Equation (H11) is solved in the same manner as equation (H6).

This results in:

$$\varphi_0 = 2 \tan^{-1} \left[ \frac{-L_0 \pm \sqrt{L_0^2 - N_0^2 + M_0^2}}{N_0 - M_0} \right] \quad (H12)$$

Again, top and bottom action results are provided.

## Disengagement Distance Between Pallet and Escape-Wheel Pivots

Figure H-2 shows the disengagement configuration of the symmetrical pin pallet runaway escapement. The pallet angle  $\psi$  equals  $\frac{\lambda}{2}$  when both pallet pins together are least advanced with respect to the escape-wheel. The center distance  $a$  is such that the escape-wheel radius  $b$  and the pallet pin radius  $r$  are collinear.

The disengagement center distance  $a_{\text{dis}}$  is determined with the help of the cosine law:

$$(b + r)^2 = a_{\text{dis}}^2 + c^2 - 2a_{\text{dis}}(c) \cos \left( \frac{\lambda}{2} \right) \quad (\text{H13})$$

From the solution of the quadratic equation, one finds:

$$a_{\text{dis}} = (c) \cos \left( \frac{\lambda}{2} \right) + \sqrt{[(c) \cos \left( \frac{\lambda}{2} \right)]^2 - [c^2 - (b + r)^2]} \quad (\text{H14})$$



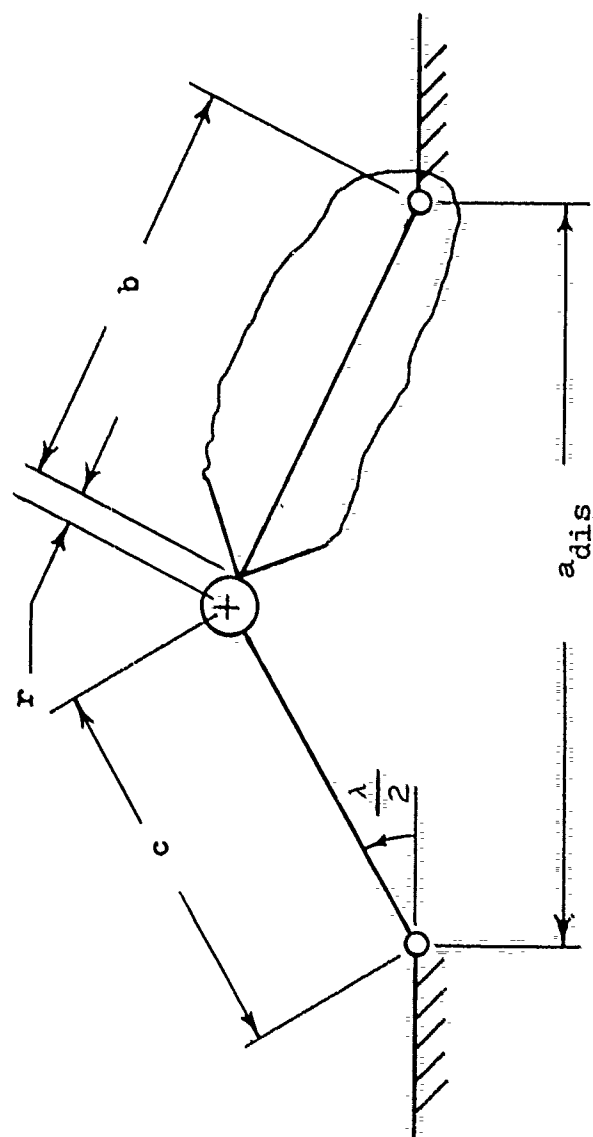


Figure H2. Disengagement condition

APPENDIX I

COMPUTER OUTPUT FOR STANDARD CONFIGURATION  
WITH  $\mu = .3$  AND  $\varepsilon = .25$

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A#	.19310	R#	.15934	C#	.30000E+00	IPAL#	.91000E-07	ISTAR#	.17000E-07	ALPHA#	40.0000
TORQUE#	.17700E-01	COFR#									
EREST#	.25	LAMBDA#	109.337	DELTA#	40.000						
Cycle No. 1											
COUPLED MOTION											
T#	0.00000	PHI#	135.000	PHIDOT#	0.000	G#	-.0457	GDOT#	0.000	PSIN#	42.412
T#	0.00000	PHI#	135.000	PHIDOT#	.044	G#	-.0457	GDOT#	.014	PSIN#	42.412
T#	0.00000	PHI#	135.000	PHIDOT#	.151	G#	-.0457	GDOT#	.012	PSIN#	42.412
T#	0.00000	PHI#	135.000	PHIDOT#	.210	G#	-.0457	GDOT#	.007	PSIN#	42.412
T#	0.00001	PHI#	135.000	PHIDOT#	.284	G#	-.0457	GDOT#	.001	PSIN#	42.412
T#	0.00001	PHI#	135.000	PHIDOT#	.421	G#	-.0457	GDOT#	.000	PSIN#	42.412
T#	0.00001	PHI#	135.000	PHIDOT#	.554	G#	-.0457	GDOT#	.000	PSIN#	42.412
T#	0.00002	PHI#	135.000	PHIDOT#	.827	G#	-.0457	GDOT#	.000	PSIN#	42.412
T#	0.00002	PHI#	135.000	PHIDOT#	1.047	G#	-.0457	GDOT#	.000	PSIN#	42.412
T#	0.00004	PHI#	135.002	PHIDOT#	1.637	G#	-.0457	GDOT#	.000	PSIN#	42.412
T#	0.00005	PHI#	135.003	PHIDOT#	2.177	G#	-.0457	GDOT#	.000	PSIN#	42.412
T#	0.00007	PHI#	135.007	PHIDOT#	3.254	G#	-.0456	GDOT#	.000	PSIN#	42.412
T#	0.00010	PHI#	135.012	PHIDOT#	4.335	G#	-.0456	GDOT#	.000	PSIN#	42.412
T#	0.00015	PHI#	135.024	PHIDOT#	6.494	G#	-.0456	GDOT#	.000	PSIN#	42.412
T#	0.00020	PHI#	135.050	PHIDOT#	8.639	G#	-.0455	GDOT#	.000	PSIN#	42.412
T#	0.00030	PHI#	135.111	PHIDOT#	12.913	G#	-.0453	GDOT#	.000	PSIN#	42.412
T#	0.00040	PHI#	135.198	PHIDOT#	17.149	G#	-.0449	GDOT#	.000	PSIN#	42.412
T#	0.00050	PHI#	135.304	PHIDOT#	21.311	G#	-.0445	GDOT#	.000	PSIN#	42.412
T#	0.00060	PHI#	135.442	PHIDOT#	25.411	G#	-.0440	GDOT#	.000	PSIN#	42.412
T#	0.00070	PHI#	135.599	PHIDOT#	29.433	G#	-.0434	GDOT#	.000	PSIN#	42.412
T#	0.00080	PHI#	135.779	PHIDOT#	33.364	G#	-.0427	GDOT#	.000	PSIN#	42.412
T#	0.00090	PHI#	135.941	PHIDOT#	37.180	G#	-.0420	GDOT#	.000	PSIN#	42.412
T#	0.00100	PHI#	136.205	PHIDOT#	40.911	G#	-.0411	GDOT#	.000	PSIN#	42.412
T#	0.00110	PHI#	136.449	PHIDOT#	44.522	G#	-.0402	GDOT#	.000	PSIN#	42.412
T#	0.00120	PHI#	136.715	PHIDOT#	48.014	G#	-.0392	GDOT#	.000	PSIN#	42.412
T#	0.00130	PHI#	136.999	PHIDOT#	51.397	G#	-.0381	GDOT#	.000	PSIN#	42.412
T#	0.00140	PHI#	137.303	PHIDOT#	54.659	G#	-.0369	GDOT#	.000	PSIN#	42.412
T#	0.00150	PHI#	137.626	PHIDOT#	57.804	G#	-.0356	GDOT#	.000	PSIN#	42.412
T#	0.00160	PHI#	137.966	PHIDOT#	60.837	G#	-.0343	GDOT#	.000	PSIN#	42.412
T#	0.00170	PHI#	138.322	PHIDOT#	63.759	G#	-.0329	GDOT#	.000	PSIN#	42.412
T#	0.00180	PHI#	138.696	PHIDOT#	66.554	G#	-.0314	GDOT#	.000	PSIN#	42.412
T#	0.00190	PHI#	139.045	PHIDOT#	69.261	G#	-.0299	GDOT#	.000	PSIN#	42.412
T#	0.00200	PHI#	139.469	PHIDOT#	71.864	G#	-.0282	GDOT#	.000	PSIN#	42.412
T#	0.00210	PHI#	139.903	PHIDOT#	74.372	G#	-.0264	GDOT#	.000	PSIN#	42.412
T#	0.00220	PHI#	140.341	PHIDOT#	76.794	G#	-.0248	GDOT#	.000	PSIN#	42.412
T#	0.00230	PHI#	140.788	PHIDOT#	79.125	G#	-.0230	GDOT#	.000	PSIN#	42.412
T#	0.00240	PHI#	141.244	PHIDOT#	81.361	G#	-.0211	GDOT#	.000	PSIN#	42.412
T#	0.00250	PHI#	141.721	PHIDOT#	83.564	G#	-.0192	GDOT#	.000	PSIN#	42.412
T#	0.00260	PHI#	142.205	PHIDOT#	85.681	G#	-.0172	GDOT#	.000	PSIN#	42.412
T#	0.00270	PHI#	142.702	PHIDOT#	87.744	G#	-.0152	GDOT#	.000	PSIN#	42.412
T#	0.00280	PHI#	143.211	PHIDOT#	89.741	G#	-.0131	GDOT#	.000	PSIN#	42.412
T#	0.00290	PHI#	143.731	PHIDOT#	91.692	G#	-.0109	GDOT#	.000	PSIN#	42.412
T#	0.00300	PHI#	144.261	PHIDOT#	93.594	G#	-.0087	GDOT#	.000	PSIN#	42.412
T#	0.00310	PHI#	144.803	PHIDOT#	95.467	G#	-.0064	GDOT#	.000	PSIN#	42.412
T#	0.00320	PHI#	145.355	PHIDOT#	97.292	G#	-.0041	GDOT#	.000	PSIN#	42.412
T#	0.00330	PHI#	145.918	PHIDOT#	99.091	G#	-.0017	GDOT#	.000	PSIN#	42.412

Appendix I

Std. Config.  
μ = .3, σ = .25

PHITOT = 11.691

1504

一一一

FREE MOTION  
T .00384 PHIZ 193.945 PHO01=-193.970 PSI= 315.548 PS1007= 26.138 PH1017= 18.945

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[illegible]

T	.00430	PMI	193.292	PMI001	7.201	G	-.0413	GOOT	1.108	PSIO	316.071	PSIO01	-6.435	PMI01	14.242
T	.00432	PMI	193.306	PMI001	11.712	G	-.0443	GOOT	1.643	PSIO	316.059	PSIO01	-10.137	PMI01	14.306
T	.00435	PMI	193.326	PMI001	15.513	G	-.0412	GOOT	2.178	PSIO	316.042	PSIO01	-13.439	PMI01	14.326
T	.00440	PMI	193.341	PMI001	23.072	G	-.0411	GOOT	3.264	PSIO	315.994	PSIO01	-20.037	PMI01	14.361
T	.00445	PMI	193.358	PMI001	30.573	G	-.0409	GOOT	4.306	PSIO	315.927	PSIO01	-24.627	PMI01	14.454
T	.00450	PMI	193.556	PMI001	37.973	G	-.0407	GOOT	5.343	PSIO	315.841	PSIO01	-31.206	PMI01	14.556
T	.00455	PMI	193.676	PMI001	45.254	G	-.0404	GOOT	6.411	PSIO	315.737	PSIO01	-39.770	PMI01	14.676
T	.00465	PMI	193.976	PMI001	59.394	G	-.0396	GOOT	8.441	PSIO	315.621	PSIO01	-52.845	PMI01	14.976
T	.00475	PMI	194.355	PMI001	72.823	G	-.0387	GOOT	10.506	PSIO	315.471	PSIO01	-65.824	PMI01	19.355
T	.00485	PMI	194.809	PMI001	85.990	G	-.0375	GOOT	12.476	PSIO	315.271	PSIO01	-78.685	PMI01	19.809
T	.00495	PMI	195.331	PMI001	96.971	G	-.0362	GOOT	14.342	PSIO	315.030	PSIO01	-91.392	PMI01	20.331
T	.00505	PMI	195.918	PMI001	107.454	G	-.0347	GOOT	16.216	PSIO	313.670	PSIO01	-103.914	PMI01	20.914
T	.00515	PMI	196.561	PMI001	116.754	G	-.0329	GOOT	17.931	PSIO	313.040	PSIO01	-114.222	PMI01	21.561
T	.00525	PMI	197.253	PMI001	124.804	G	-.0311	GOOT	19.642	PSIO	312.339	PSIO01	-124.274	PMI01	22.253
T	.00535	PMI	197.988	PMI001	131.564	G	-.0290	GOOT	21.223	PSIO	311.570	PSIO01	-140.042	PMI01	22.988
T	.00545	PMI	198.758	PMI001	137.014	G	-.0268	GOOT	22.710	PSIO	310.735	PSIO01	-151.482	PMI01	23.758
T	.00555	PMI	199.556	PMI001	141.154	G	-.0245	GOOT	24.101	PSIO	309.835	PSIO01	-167.562	PMI01	24.556
T	.00565	PMI	200.373	PMI001	144.013	G	-.0220	GOOT	25.392	PSIO	308.873	PSIO01	-173.244	PMI01	25.373
T	.00575	PMI	201.204	PMI001	145.627	G	-.0194	GOOT	26.582	PSIO	307.851	PSIO01	-173.505	PMI01	26.264
T	.00585	PMI	202.040	PMI001	146.957	G	-.0167	GOOT	27.671	PSIO	306.771	PSIO01	-193.307	PMI01	27.040
T	.00595	PMI	202.875	PMI001	147.974	G	-.0139	GOOT	28.656	PSIO	305.637	PSIO01	-207.526	PMI01	27.875
T	.00605	PMI	203.704	PMI001	148.652	G	-.0110	GOOT	29.540	PSIO	304.450	PSIO01	-219.440	PMI01	28.764
T	.00615	PMI	204.520	PMI001	149.000	G	-.0080	GOOT	30.323	PSIO	303.215	PSIO01	-219.732	PMI01	29.520
T	.00625	PMI	205.318	PMI001	149.505	G	-.0049	GOOT	31.006	PSIO	301.933	PSIO01	-227.487	PMI01	30.318
T	.00635	PMI	206.094	PMI001	149.274	G	-.0018	GOOT	31.581	PSIO	300.609	PSIO01	-236.697	PMI01	31.094
T	.00645	PMI	206.844	PMI001	148.397	G	.0014	GOOT	32.052	PSIO	299.245	PSIO01	-243.357	PMI01	31.844

T	.00645	PMI	126.844	PMI001	124.397	PSI	48.582	PSIO01	-241.357	PMI01	31.844
T	.00646	PMI	126.920	PMI001	124.808	PSI	48.444	PSIO01	-241.357	PMI01	31.920
T	.00647	PMI	127.003	PMI001	124.220	PSI	48.305	PSIO01	-241.357	PMI01	32.003
T	.00648	PMI	127.091	PMI001	124.632	PSI	48.167	PSIO01	-241.357	PMI01	32.091
T	.00649	PMI	127.186	PMI001	125.044	PSI	48.029	PSIO01	-241.357	PMI01	32.166
T	.00650	PMI	127.266	PMI001	125.456	PSI	47.890	PSIO01	-241.357	PMI01	32.246
T	.00651	PMI	127.393	PMI001	125.867	PSI	47.752	PSIO01	-241.357	PMI01	32.323
T	.00652	PMI	127.505	PMI001	126.279	PSI	47.614	PSIO01	-241.357	PMI01	32.395
T	.00653	PMI	127.623	PMI001	126.691	PSI	47.476	PSIO01	-241.357	PMI01	32.473
T	.00654	PMI	127.747	PMI001	127.103	PSI	47.337	PSIO01	-241.357	PMI01	32.547
T	.00655	PMI	127.878	PMI001	127.514	PSI	47.199	PSIO01	-241.357	PMI01	32.623
T	.00656	PMI	128.014	PMI001	127.926	PSI	47.061	PSIO01	-241.357	PMI01	32.698
T	.00657	PMI	128.156	PMI001	128.338	PSI	46.922	PSIO01	-241.357	PMI01	32.774
T	.00658	PMI	128.304	PMI001	128.750	PSI	46.784	PSIO01	-241.357	PMI01	32.850
T	.00659	PMI	128.458	PMI001	129.161	PSI	46.646	PSIO01	-241.357	PMI01	32.926
T	.00660	PMI	128.518	PMI001	129.573	PSI	46.507	PSIO01	-241.357	PMI01	33.001
T	.00661	PMI	128.784	PMI001	129.985	PSI	46.369	PSIO01	-241.357	PMI01	33.076
T	.00662	PMI	128.956	PMI001	130.397	PSI	46.231	PSIO01	-241.357	PMI01	33.151
T	.00663	PMI	129.134	PMI001	130.808	PSI	46.093	PSIO01	-241.357	PMI01	33.226
T	.00664	PMI	129.318	PMI001	131.220	PSI	45.954	PSIO01	-241.357	PMI01	33.301
T	.00665	PMI	129.508	PMI001	131.632	PSI	45.816	PSIO01	-241.357	PMI01	33.376
T	.00666	PMI	129.704	PMI001	132.044	PSI	45.678	PSIO01	-241.357	PMI01	33.451
T	.00667	PMI	129.906	PMI001	132.456	PSI	45.539	PSIO01	-241.357	PMI01	33.526
T	.00668	PMI	130.114	PMI001	132.867	PSI	45.401	PSIO01	-241.357	PMI01	33.601
T	.00669	PMI	130.327	PMI001	133.279	PSI	45.263	PSIO01	-241.357	PMI01	33.676
T	.00670	PMI	130.547	PMI001	133.691	PSI	45.125	PSIO01	-241.357	PMI01	33.751
T	.00671	PMI	130.773	PMI001	134.103	PSI	44.986	PSIO01	-241.357	PMI01	33.826
T	.00672	PMI	131.004	PMI001	134.514	PSI	44.848	PSIO01	-241.357	PMI01	33.901
T	.00673	PMI	131.242	PMI001	134.926	PSI	44.710	PSIO01	-241.357	PMI01	33.976
T	.00674	PMI	131.486	PMI001	135.338	PSI	44.571	PSIO01	-241.357	PMI01	34.051
T	.00675	PMI	131.735	PMI001	135.750	PSI	44.433	PSIO01	-241.357	PMI01	34.126
T	.00676	PMI	132.000	PMI001	136.161	PSI	44.295	PSIO01	-241.357	PMI01	34.201
T	.00677	PMI	132.252	PMI001	136.573	PSI	44.157	PSIO01	-241.357	PMI01	34.276
T	.00678	PMI	132.520	PMI001	136.985	PSI	44.018	PSIO01	-241.357	PMI01	34.351
T	.00679	PMI	132.793	PMI001	137.397	PSI	43.880	PSIO01	-241.357	PMI01	34.426

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Cycle No. 2									
IMPACT									
<p>VP = -7.044 VS = -21.769</p>									
<p>FREE MOTION</p>									
T = .00680	PMI = 133.072	PMOIT = 492.808	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00681	PMI = 133.368	PMOIT = 503.280	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00682	PMI = 133.629	PMOIT = 513.632	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00683	PMI = 133.9-6	PMOIT = 524.044	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00684	PMI = 134.250	PMOIT = 534-56	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00685	PMI = 134.559	PMOIT = 544.867	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00686	PMI = 134.874	PMOIT = 555.279	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00687	PMI = 135.185	PMOIT = 565.691	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00688	PMI = 135.522	PMOIT = 576.103	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
VP = -14.102 VS = 44.710									
IMPACT									
<p>VP = -7.044 VS = -21.769</p>									
<p>FREE MOTION</p>									
T = .00689	PMI = 135.365	PMOIT = -270.043	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00690	PMI = 135.213	PMOIT = -259.631	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
VP = -7.092 VS = -19.850									
IMPACT									
<p>VP = -7.105 VS = -19.918</p>									
<p>FREE MOTION</p>									
T = .00690	PMI = 135.213	PMOIT = -259.631	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00691	PMI = 135.067	PMOIT = -249.220	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
VP = -7.105 VS = -19.918									
IMPACT									
<p>VP = -7.043 VS = -19.684</p>									
<p>FREE MOTION</p>									
T = .00691	PMI = 135.067	PMOIT = -249.220	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00692	PMI = 134.927	PMOIT = -238.808	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00693	PMI = 134.793	PMOIT = -228.396	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00694	PMI = 134.665	PMOIT = -217.986	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00695	PMI = 134.544	PMOIT = -207.573	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00696	PMI = 134.428	PMOIT = -197.161	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
T = .00697	PMI = 134.318	PMOIT = -186.749	PSI = 42.635	PSIOT = -120.910	PMIOT = 40.522				
VP = -7.043 VS = -19.684									
IMPACT									

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VP= -5.503	VS= -7.432	PHI= 133.435	DPHIF= -117.116	PSI= 40.419	OPSIF= -94.464	PHITOT= 38.435
FREE MOTION						
T= .00720	PHI= 133.435	PHOOT= -117.116	PSI= 40.419	PSIDOT= -94.464	PHITOT= 38.435	
T= .00721	PHI= 133.370	PHOOT= -106.706	PSI= 40.356	PSIDOT= -94.464	PHITOT= 38.370	
VP= -5.504	VS= -7.432					
FREE MOTION						
T= .00721	PHI= 133.370	PHOOT= -106.706	PSI= 40.344	PSIDOT= -94.464	PHITOT= 38.370	
T= .00722	PHI= 133.312	PHOOT= -96.292	PSI= 40.310	PSIDOT= -94.464	PHITOT= 38.312	
VP= -5.505	VS= -6.687					
FREE MOTION						
T= .00722	PHI= 133.312	PHOOT= -96.292	PSI= 40.310	PSIDOT= -94.464	PHITOT= 38.312	
T= .00723	PHI= 133.260	PHOOT= -85.880	PSI= 40.256	PSIDOT= -94.464	PHITOT= 38.260	
VP= -5.506	VS= -5.947					
FREE MOTION						
T= .00723	PHI= 133.260	PHOOT= -85.880	PSI= 40.256	PSIDOT= -94.464	PHITOT= 38.260	
T= .00724	PHI= 133.214	PHOOT= -75.468	PSI= 40.202	PSIDOT= -94.464	PHITOT= 38.214	
VP= -5.503	VS= -5.214					
IMPACT						
VP= -5.641	VS= -5.533	PHI= 133.214	DPHIF= -80.092	PSI= 40.202	OPSIF= -93.736	PHITOT= 38.214
COUPLED MOTION						
T= .00724	PHI= 133.214	PHIDOT= -80.092	G= -0.0522	GDOT= -16.592	PSID= 40.204	PSIDOT= -94.974
T= .00724	PHI= 132.830	PHIDOT= -53.464	G= -0.0534	GDOT= -10.990	PSID= 39.754	PSIDOT= -67.227
T= .00744	PHI= 132.604	PHIDOT= -25.344	G= -0.0544	GDOT= -5.146	PSID= 39.414	PSIDOT= -29.172
T= .00744	PHI= 132.573	PHIDOT= -18.176	G= -0.0545	GDOT= -3.715	PSID= 39.456	PSIDOT= -20.880
T= .00749	PHI= 132.552	PHIDOT= -10.461	G= -0.0546	GDOT= -2.240	PSID= 39.432	PSIDOT= -17.542
T= .00750	PHI= 132.545	PHIDOT= -7.344	G= -0.0547	GDOT= -1.581	PSID= 39.424	PSIDOT= -14.432
T= .00751	PHI= 132.541	PHIDOT= -3.731	G= -0.0547	GDOT= -0.762	PSID= 39.420	PSIDOT= -7.281
T= .00752	PHI= 132.540	PHIDOT= -1.922	G= -0.0547	GDOT= -0.393	PSID= 39.419	PSIDOT= -2.205
T= .00753	PHI= 132.540	PHIDOT= -1.117	G= -0.0547	GDOT= -0.231	PSID= 39.418	PSIDOT= -1.129
T= .00753	PHI= 132.540	PHIDOT= -0.911	G= -0.0547	GDOT= -0.189	PSID= 39.418	PSIDOT= -0.105
T= .00753	PHI= 132.540	PHIDOT= -0.751	G= -0.0547	GDOT= -0.151	PSID= 39.418	PSIDOT= -0.078
T= .00753	PHI= 132.540	PHIDOT= -0.607	G= -0.0547	GDOT= -0.108	PSID= 39.418	PSIDOT= -0.052
T= .00754	PHI= 132.540	PHIDOT= -0.493	G= -0.0547	GDOT= -0.080	PSID= 39.418	PSIDOT= -0.039
T= .00754	PHI= 132.540	PHIDOT= -0.400	G= -0.0547	GDOT= -0.063	PSID= 39.418	PSIDOT= -0.031
T= .00755	PHI= 132.541	PHIDOT= -0.328	G= -0.0547	GDOT= -0.051	PSID= 39.419	PSIDOT= -0.025
T= .00755	PHI= 132.542	PHIDOT= -0.267	G= -0.0547	GDOT= -0.040	PSID= 39.420	PSIDOT= -0.020
T= .00756	PHI= 132.542	PHIDOT= -0.213	G= -0.0547	GDOT= -0.033	PSID= 39.421	PSIDOT= -0.016
T= .00758	PHI= 132.544	PHIDOT= -0.164	G= -0.0546	GDOT= -0.026	PSID= 39.422	PSIDOT= -0.012
T= .00759	PHI= 132.546	PHIDOT= -0.120	G= -0.0546	GDOT= -0.020	PSID= 39.425	PSIDOT= -0.009
T= .00761	PHI= 132.551	PHIDOT= -0.080	G= -0.0546	GDOT= -0.015	PSID= 39.431	PSIDOT= -0.007
T= .00764	PHI= 132.559	PHIDOT= -0.048	G= -0.0546	GDOT= -0.010	PSID= 39.439	PSIDOT= -0.005
T= .00769	PHI= 132.579	PHIDOT= -0.028	G= -0.0546	GDOT= -0.006	PSID= 39.463	PSIDOT= -0.003
T= .00774	PHI= 132.606	PHIDOT= -0.016	G= -0.0544	GDOT= -0.003	PSID= 39.494	PSIDOT= -0.001
T= .00779	PHI= 132.641	PHIDOT= -0.008	G= -0.0543	GDOT= -0.001	PSID= 39.536	PSIDOT= -0.000
T= .00784	PHI= 132.683	PHIDOT= -0.004	G= -0.0542	GDOT= -0.000	PSID= 39.587	PSIDOT= -0.000
T= .00794	PHI= 132.787	PHIDOT= -0.002	G= -0.0533	GDOT= -0.000	PSID= 39.704	PSIDOT= -0.000
T= .00804	PHI= 132.920	PHIDOT= -0.001	G= -0.0533	GDOT= -0.000	PSID= 39.859	PSIDOT= -0.000
T= .00814	PHI= 133.091	PHIDOT= -0.000	G= -0.0527	GDOT= -0.000	PSID= 40.047	PSIDOT= -0.000
T= .00824	PHI= 133.269	PHIDOT= -0.000	G= -0.0520	GDOT= -0.000	PSID= 40.268	PSIDOT= -0.000
T= .00834	PHI= 133.481	PHIDOT= -0.000	G= -0.0513	GDOT= -0.000	PSID= 40.523	PSIDOT= -0.000
T= .00844	PHI= 133.719	PHIDOT= -0.000	G= -0.0504	GDOT= -0.000	PSID= 40.810	PSIDOT= -0.000
T= .00854	PHI= 133.981	PHIDOT= -0.000	G= -0.0494	GDOT= -0.000	PSID= 41.131	PSIDOT= -0.000
T= .00864	PHI= 134.266	PHIDOT= -0.000	G= -0.0484	GDOT= -0.000	PSID= 41.484	PSIDOT= -0.000



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T	.00874	PHI	136.574	PHINDOT	55.527	G	-.00473	GOOT	11.611	PSID	41.869	PSINDOT	70.100	PHINDOT	39.902
T	.00884	PHI	136.902	PHINDOT	59.137	G	-.00460	GOOT	12.654	PSID	42.287	PSINDOT	75.729	PHINDOT	40.251
T	.00894	PHI	137.251	PHINDOT	62.565	G	-.00447	GOOT	13.472	PSID	42.737	PSINDOT	81.328	PHINDOT	40.519
T	.00904	PHI	137.519	PHINDOT	65.931	G	-.00433	GOOT	14.267	PSID	43.219	PSINDOT	86.897	PHINDOT	41.005
T	.00914	PHI	137.805	PHINDOT	69.326	G	-.00419	GOOT	15.038	PSID	43.733	PSINDOT	92.437	PHINDOT	41.409
T	.00924	PHI	138.005	PHINDOT	71.881	G	-.00403	GOOT	15.786	PSID	44.278	PSINDOT	97.948	PHINDOT	41.829
T	.00934	PHI	138.229	PHINDOT	74.486	G	-.00387	GOOT	16.512	PSID	44.855	PSINDOT	103.431	PHINDOT	42.264
T	.00944	PHI	138.469	PHINDOT	77.138	G	-.00370	GOOT	17.216	PSID	45.463	PSINDOT	108.886	PHINDOT	42.715
T	.00954	PHI	138.715	PHINDOT	79.881	G	-.00353	GOOT	17.899	PSID	46.103	PSINDOT	114.317	PHINDOT	43.179
T	.00964	PHI	138.971	PHINDOT	82.684	G	-.00336	GOOT	18.562	PSID	46.773	PSINDOT	119.723	PHINDOT	43.657
T	.00974	PHI	139.237	PHINDOT	85.539	G	-.00319	GOOT	19.206	PSID	47.474	PSINDOT	125.106	PHINDOT	44.148
T	.00984	PHI	139.512	PHINDOT	88.444	G	-.00302	GOOT	19.821	PSID	48.207	PSINDOT	130.470	PHINDOT	44.652
T	.00994	PHI	139.797	PHINDOT	91.400	G	-.00285	GOOT	20.418	PSID	48.969	PSINDOT	135.815	PHINDOT	45.167
T	.01004	PHI	140.092	PHINDOT	94.407	G	-.00268	GOOT	21.009	PSID	49.763	PSINDOT	141.143	PHINDOT	45.694
T	.01014	PHI	140.397	PHINDOT	97.454	G	-.00251	GOOT	21.593	PSID	50.587	PSINDOT	146.458	PHINDOT	46.231
T	.01024	PHI	140.712	PHINDOT	100.549	G	-.00234	GOOT	22.162	PSID	51.441	PSINDOT	151.761	PHINDOT	46.779
T	.01034	PHI	141.037	PHINDOT	103.684	G	-.00217	GOOT	22.726	PSID	52.326	PSINDOT	157.055	PHINDOT	47.339
T	.01044	PHI	141.372	PHINDOT	106.869	G	-.00200	GOOT	23.285	PSID	53.241	PSINDOT	162.341	PHINDOT	47.906
T	.01054	PHI	141.717	PHINDOT	110.104	G	-.00183	GOOT	23.839	PSID	54.186	PSINDOT	167.622	PHINDOT	48.484
T	.01064	PHI	142.072	PHINDOT	113.389	G	-.00166	GOOT	24.388	PSID	55.162	PSINDOT	172.901	PHINDOT	49.072
T	.01074	PHI	142.437	PHINDOT	116.724	G	-.00149	GOOT	24.932	PSID	56.167	PSINDOT	178.179	PHINDOT	49.669
T	.01084	PHI	142.812	PHINDOT	120.109	G	-.00132	GOOT	25.471	PSID	57.203	PSINDOT	183.459	PHINDOT	50.275
T	.01094	PHI	143.197	PHINDOT	123.544	G	-.00115	GOOT	26.005	PSID	58.270	PSINDOT	188.742	PHINDOT	50.891
T	.01104	PHI	143.592	PHINDOT	127.029	G	-.00098	GOOT	26.534	PSID	59.364	PSINDOT	194.031	PHINDOT	51.515
T	.01114	PHI	144.007	PHINDOT	130.564	G	-.00081	GOOT	27.058	PSID	60.493	PSINDOT	199.328	PHINDOT	52.151

FREE MOTION

T	.01114	PHI	144.432	PHINDOT	134.159	PSI	311.156	PSINDOT	199.328	PHINDOT	51.515
T	.01124	PHI	144.867	PHINDOT	137.704	PSI	311.270	PSINDOT	199.328	PHINDOT	51.515
T	.01134	PHI	145.312	PHINDOT	141.309	PSI	311.345	PSINDOT	199.328	PHINDOT	51.515
T	.01144	PHI	145.767	PHINDOT	144.974	PSI	311.413	PSINDOT	199.328	PHINDOT	51.515
T	.01154	PHI	146.232	PHINDOT	148.699	PSI	311.477	PSINDOT	199.328	PHINDOT	51.515
T	.01164	PHI	146.707	PHINDOT	152.484	PSI	311.536	PSINDOT	199.328	PHINDOT	51.515
T	.01174	PHI	147.192	PHINDOT	156.329	PSI	311.591	PSINDOT	199.328	PHINDOT	51.515
T	.01184	PHI	147.687	PHINDOT	160.234	PSI	311.642	PSINDOT	199.328	PHINDOT	51.515
T	.01194	PHI	148.192	PHINDOT	164.199	PSI	311.689	PSINDOT	199.328	PHINDOT	51.515
T	.01204	PHI	148.707	PHINDOT	168.224	PSI	311.732	PSINDOT	199.328	PHINDOT	51.515
T	.01214	PHI	149.232	PHINDOT	172.309	PSI	311.771	PSINDOT	199.328	PHINDOT	51.515
T	.01224	PHI	149.767	PHINDOT	176.454	PSI	311.806	PSINDOT	199.328	PHINDOT	51.515
T	.01234	PHI	150.312	PHINDOT	180.659	PSI	311.837	PSINDOT	199.328	PHINDOT	51.515
T	.01244	PHI	150.867	PHINDOT	184.924	PSI	311.864	PSINDOT	199.328	PHINDOT	51.515
T	.01254	PHI	151.432	PHINDOT	189.249	PSI	311.887	PSINDOT	199.328	PHINDOT	51.515
T	.01264	PHI	152.007	PHINDOT	193.634	PSI	311.906	PSINDOT	199.328	PHINDOT	51.515
T	.01274	PHI	152.592	PHINDOT	198.079	PSI	311.921	PSINDOT	199.328	PHINDOT	51.515
T	.01284	PHI	153.187	PHINDOT	202.584	PSI	311.932	PSINDOT	199.328	PHINDOT	51.515
T	.01294	PHI	153.792	PHINDOT	207.149	PSI	311.939	PSINDOT	199.328	PHINDOT	51.515
T	.01304	PHI	154.407	PHINDOT	211.774	PSI	311.942	PSINDOT	199.328	PHINDOT	51.515
T	.01314	PHI	155.032	PHINDOT	216.459	PSI	311.941	PSINDOT	199.328	PHINDOT	51.515
T	.01324	PHI	155.667	PHINDOT	221.204	PSI	311.936	PSINDOT	199.328	PHINDOT	51.515
T	.01334	PHI	156.312	PHINDOT	226.009	PSI	311.927	PSINDOT	199.328	PHINDOT	51.515
T	.01344	PHI	156.967	PHINDOT	230.874	PSI	311.914	PSINDOT	199.328	PHINDOT	51.515
T	.01354	PHI	157.632	PHINDOT	235.799	PSI	311.897	PSINDOT	199.328	PHINDOT	51.515
T	.01364	PHI	158.307	PHINDOT	240.784	PSI	311.876	PSINDOT	199.328	PHINDOT	51.515
T	.01374	PHI	158.992	PHINDOT	245.829	PSI	311.851	PSINDOT	199.328	PHINDOT	51.515
T	.01384	PHI	159.687	PHINDOT	250.934	PSI	311.822	PSINDOT	199.328	PHINDOT	51.515
T	.01394	PHI	160.392	PHINDOT	256.099	PSI	311.789	PSINDOT	199.328	PHINDOT	51.515
T	.01404	PHI	161.107	PHINDOT	261.324	PSI	311.752	PSINDOT	199.328	PHINDOT	51.515
T	.01414	PHI	161.832	PHINDOT	266.609	PSI	311.711	PSINDOT	199.328	PHINDOT	51.515
T	.01424	PHI	162.567	PHINDOT	271.954	PSI	311.666	PSINDOT	199.328	PHINDOT	51.515
T	.01434	PHI	163.312	PHINDOT	277.359	PSI	311.617	PSINDOT	199.328	PHINDOT	51.515
T	.01444	PHI	164.067	PHINDOT	282.824	PSI	311.564	PSINDOT	199.328	PHINDOT	51.515
T	.01454	PHI	164.832	PHINDOT	288.349	PSI	311.507	PSINDOT	199.328	PHINDOT	51.515
T	.01464	PHI	165.607	PHINDOT	293.934	PSI	311.446	PSINDOT	199.328	PHINDOT	51.515
T	.01474	PHI	166.392	PHINDOT	299.579	PSI	311.381	PSINDOT	199.328	PHINDOT	51.515
T	.01484	PHI	167.187	PHINDOT	305.284	PSI	311.312	PSINDOT	199.328	PHINDOT	51.515
T	.01494	PHI	167.992	PHINDOT	311.049	PSI	311.239	PSINDOT	199.328	PHINDOT	51.515
T	.01504	PHI	168.807	PHINDOT	316.884	PSI	311.162	PSINDOT	199.328	PHINDOT	51.515
T	.01514	PHI	169.632	PHINDOT	322.779	PSI	311.081	PSINDOT	199.328	PHINDOT	51.515
T	.01524	PHI	170.467	PHINDOT	328.734	PSI	311.006	PSINDOT	199.328	PHINDOT	51.515
T	.01534	PHI	171.312	PHINDOT	334.749	PSI	310.927	PSINDOT	199.328	PHINDOT	51.515
T	.01544	PHI	172.167	PHINDOT	340.824	PSI	310.844	PSINDOT	199.328	PHINDOT	51.515
T	.01554	PHI	173.032	PHINDOT	346.959	PSI	310.757	PSINDOT	199.328	PHINDOT	51.515
T	.01564	PHI	173.907	PHINDOT	353.154	PSI	310.666	PSINDOT	199.328	PHINDOT	51.515
T	.01574	PHI	174.792	PHINDOT	359.409	PSI	310.571	PSINDOT	199.328	PHINDOT	51.515
T	.01584	PHI	175.687	PHINDOT	365.724	PSI	310.472	PSINDOT	199.328	PHINDOT	51.515
T	.01594	PHI	176.592	PHINDOT	372.099	PSI	310.370	PSINDOT	199.328	PHINDOT	51.515
T	.01604	PHI	177.507	PHINDOT	378.534	PSI	310.264	PSINDOT	199.328	PHINDOT	51.515
T	.01614	PHI	178.432	PHINDOT	385.029	PSI	310.155	PSINDOT	199.328	PHINDOT	51.515
T	.01624	PHI	179.367	PHINDOT	391.584	PSI	310.042	PSINDOT	199.328	PHINDOT	51.515
T	.01634	PHI	180.312	PHINDOT	398.199	PSI	309.925	PSINDOT	199.328	PHINDOT	51.515
T	.01644	PHI	181.267	PHINDOT	404.874	PSI	309.804	PSINDOT	199.328	PHINDOT	51.515
T	.01654	PHI	182.232	PHINDOT	411.609	PSI	309.679	PSINDOT	199.328	PHINDOT	51.515
T	.01664	PHI	183.207	PHINDOT	418.404	PSI	309.550	PSINDOT	199.328	PHINDOT	51.515
T	.01674	PHI	184.192	PHINDOT	425.259	PSI	309.417	PSINDOT	199.328	PHINDOT	51.515
T	.01684	PHI	185.187	PHINDOT	432.174	PSI	309.280	PSINDOT	199.328	PHINDOT	51.515
T	.01694	PHI	186.192	PHINDOT	439.149	PSI	309.139	PSINDOT	199.328	PHINDOT	51.515
T	.01704	PHI	187.207	PHINDOT	446.184	PSI	308.994	PSINDOT	199.328	PHINDOT	51.515
T	.01714	PHI	188.232	PHINDOT	453.279	PSI	308.845	PSINDOT	199.328	PHINDOT	51.515
T	.01724	PHI	189.267	PHINDOT	460.434	PSI	308.692	PSINDOT	199.328	PHINDOT	51.515
T	.01734	PHI	190.312	PHINDOT	467.649	PSI	308.535	PSINDOT	199.328	PHINDOT	51.515
T	.01744	PHI	191.367	PHINDOT	474.924	PSI	308.374	PSINDOT	199.328	PHINDOT	51.515
T	.01754	PHI	192.432	PHINDOT	482.259	PSI	308.209	PSINDOT	199.328	PHINDOT	51.515
T	.01764	PHI	193.507	PHINDOT	489.654	PSI	308.040	PSINDOT	199.328	PHINDOT	51.515
T	.01774	PHI	194.592	PHINDOT	497.109	PSI	307.867	PSINDOT	199.328	PHINDOT	51.515
T	.01784	PHI	195.687	PHINDOT	504.624	PSI	307.690	PSINDOT	199.328	PHINDOT	51.515
T	.01794	PHI	196.792	PHINDOT	512.199	PSI	307.509	PSINDOT	199.328	PHINDOT	51.515
T	.01804	PHI	197.907	PHINDOT	519.834	PSI	307.324	PSINDOT	199.328	PHINDOT	51.515
T	.01814	PHI	199.032	PHINDOT	527.529	PSI	307.135	PSINDOT	199.328	PHINDOT	51.515
T	.01824	PHI	200.167	PHINDOT	535.284	PSI	306.942	PSINDOT	199.328	PHINDOT	51.515
T	.01834	PHI	201.312	PHINDOT	543.						

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T= .01153 PFI= 193.504 PPHOT= 515.198 PSI= 315.410 PSINOT= 199.326 PHTOT= 58.504  
T= .01154 PFI= 193.802 PPHOT= 526.210 PSI= 315.724 PSINOT= 199.328 PHTOT= 58.802  
VP= -18.368 VS= 42.761

IMPACT

VP= -3.579 VS= -16.857 PFI= 193.802 PPHIF= 232.037 PSI= 315.724 PSINOT= 199.326 PHTOT= 58.802

FREE MOTION

T= .01154 PFI= 193.802 PPHOT= 232.037 PSI= 315.724 PSINOT= 199.326 PHTOT= 58.802  
T= .01155 PFI= 193.672 PPHOT= 221.426 PSI= 315.747 PSINOT= 199.328 PHTOT= 58.672  
VP= -3.592 VS= -17.939

FREE MOTION

T= .01155 PFI= 193.672 PPHOT= 221.426 PSI= 315.747 PSINOT= 199.326 PHTOT= 58.672  
T= .01156 PFI= 193.548 PPHOT= 211.214 PSI= 315.769 PSINOT= 199.328 PHTOT= 58.568  
T= .01157 PFI= 193.430 PPHOT= 200.802 PSI= 315.791 PSINOT= 199.330 PHTOT= 58.430  
T= .01158 PFI= 193.312 PPHOT= 190.393 PSI= 315.814 PSINOT= 199.332 PHTOT= 58.312  
T= .01159 PFI= 193.212 PPHOT= 179.979 PSI= 315.836 PSINOT= 199.334 PHTOT= 58.212  
T= .01160 PFI= 193.112 PPHOT= 169.567 PSI= 315.858 PSINOT= 199.336 PHTOT= 58.112  
T= .01161 PFI= 193.012 PPHOT= 159.155 PSI= 315.880 PSINOT= 199.338 PHTOT= 58.012  
T= .01162 PFI= 192.930 PPHOT= 148.743 PSI= 315.903 PSINOT= 199.340 PHTOT= 57.930  
T= .01163 PFI= 192.848 PPHOT= 138.332 PSI= 315.925 PSINOT= 199.342 PHTOT= 57.848  
T= .01164 PFI= 192.771 PPHOT= 127.920 PSI= 315.947 PSINOT= 199.344 PHTOT= 57.771  
T= .01165 PFI= 192.701 PPHOT= 117.508 PSI= 315.970 PSINOT= 199.346 PHTOT= 57.701  
T= .01166 PFI= 192.637 PPHOT= 107.096 PSI= 315.992 PSINOT= 199.348 PHTOT= 57.637  
T= .01167 PFI= 192.578 PPHOT= 96.685 PSI= 316.014 PSINOT= 199.350 PHTOT= 57.578  
T= .01168 PFI= 192.526 PPHOT= 86.273 PSI= 316.036 PSINOT= 199.352 PHTOT= 57.526  
T= .01169 PFI= 192.479 PPHOT= 75.861 PSI= 316.059 PSINOT= 199.354 PHTOT= 57.479  
T= .01170 PFI= 192.439 PPHOT= 65.449 PSI= 316.081 PSINOT= 199.356 PHTOT= 57.439  
T= .01171 PFI= 192.406 PPHOT= 55.037 PSI= 316.103 PSINOT= 199.358 PHTOT= 57.406

T= .01172 PFI= 192.376 PPHOT= 44.626 PSI= 316.125 PSINOT= 199.360 PHTOT= 57.376  
T= .01173 PFI= 192.353 PPHOT= 34.214 PSI= 316.148 PSINOT= 199.362 PHTOT= 57.353  
T= .01174 PFI= 192.337 PPHOT= 23.802 PSI= 316.170 PSINOT= 199.364 PHTOT= 57.337  
T= .01175 PFI= 192.326 PPHOT= 13.390 PSI= 316.192 PSINOT= 199.366 PHTOT= 57.326  
T= .01176 PFI= 192.321 PPHOT= 2.979 PSI= 316.215 PSINOT= 199.368 PHTOT= 57.321  
T= .01177 PFI= 192.323 PPHOT= 7.433 PSI= 316.237 PSINOT= 199.370 PHTOT= 57.323  
T= .01178 PFI= 192.330 PPHOT= 17.865 PSI= 316.259 PSINOT= 199.372 PHTOT= 57.330  
T= .01179 PFI= 192.343 PPHOT= 28.297 PSI= 316.281 PSINOT= 199.374 PHTOT= 57.343  
T= .01180 PFI= 192.362 PPHOT= 38.729 PSI= 316.304 PSINOT= 199.376 PHTOT= 57.362  
T= .01181 PFI= 192.387 PPHOT= 49.161 PSI= 316.326 PSINOT= 199.378 PHTOT= 57.387  
T= .01182 PFI= 192.418 PPHOT= 59.593 PSI= 316.348 PSINOT= 199.380 PHTOT= 57.418  
T= .01183 PFI= 192.455 PPHOT= 69.025 PSI= 316.371 PSINOT= 199.382 PHTOT= 57.455  
T= .01184 PFI= 192.498 PPHOT= 78.457 PSI= 316.393 PSINOT= 199.384 PHTOT= 57.498  
T= .01185 PFI= 192.547 PPHOT= 87.889 PSI= 316.415 PSINOT= 199.386 PHTOT= 57.547  
T= .01186 PFI= 192.602 PPHOT= 97.321 PSI= 316.437 PSINOT= 199.388 PHTOT= 57.602  
T= .01187 PFI= 192.663 PPHOT= 106.753 PSI= 316.460 PSINOT= 199.390 PHTOT= 57.653  
T= .01188 PFI= 192.730 PPHOT= 121.185 PSI= 316.482 PSINOT= 199.392 PHTOT= 57.730  
T= .01189 PFI= 192.803 PPHOT= 132.374 PSI= 316.504 PSINOT= 199.394 PHTOT= 57.803  
VP= -1.414 VS= 10.436

IMPACT

VP= -0.07 VS= -3.505 PFI= 192.803 PPHIF= 44.468 PSI= 316.504 PSINOT= 199.396 PHTOT= 57.803

FREE MOTION

T= .01189 PFI= 192.803 PPHOT= 44.468 PSI= 316.504 PSINOT= 199.398 PHTOT= 57.803  
T= .01190 PFI= 192.781 PPHOT= 34.057 PSI= 316.526 PSINOT= 199.400 PHTOT= 57.781  
T= .01191 PFI= 192.764 PPHOT= 23.645 PSI= 316.548 PSINOT= 199.402 PHTOT= 57.764  
T= .01192 PFI= 192.754 PPHOT= 13.233 PSI= 316.570 PSINOT= 199.404 PHTOT= 57.754  
T= .01193 PFI= 192.749 PPHOT= 2.821 PSI= 316.592 PSINOT= 199.406 PHTOT= 57.749  
T= .01194 PFI= 192.750 PPHOT= 7.590 PSI= 316.614 PSINOT= 199.408 PHTOT= 57.750

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Y = .01195 PFI = 192.748 PMDT = 18.002 PSI = 316.504 PSINOT = -.073 PMTOT = 57.790  
T = .01196 PFI = 192.771 PMDT = 28.414 PSI = 316.504 PSINOT = -.073 PMTOT = 57.771  
T = .01197 PFI = 192.790 PMDT = 38.826 PSI = 316.504 PSINOT = -.073 PMTOT = 57.790  
VP = .007 VS = 3.059

# IMPACT

VP = .794 VS = .031  
PFI = 192.790 DPMT = .393 PSI = 316.504 DPSIF = -.853 PMTOT = 57.790

## COUPLED MOTION

T = .01197	PFI = 192.790	PMDT = 16.176	G = .393	GDT = .054	PSIO = 316.501	PSINOT = -.333	PMTOT = 57.790
T = .01207	PFI = 192.438	PMDT = 16.176	G = .393	GDT = .054	PSIO = 316.501	PSINOT = -.333	PMTOT = 57.790
T = .01217	PFI = 192.975	PMDT = 31.764	G = .0621	GDT = 4.419	PSIO = 316.344	PSINOT = -27.127	PMTOT = 57.475
T = .01227	PFI = 193.201	PMDT = 46.954	G = .0415	GDT = 6.570	PSIO = 316.150	PSINOT = -40.468	PMTOT = 57.201
T = .01237	PFI = 193.512	PMDT = 61.574	G = .0304	GDT = 8.645	PSIO = 315.940	PSINOT = -53.742	PMTOT = 56.912
T = .01247	PFI = 193.905	PMDT = 75.444	G = .0398	GDT = 10.752	PSIO = 315.534	PSINOT = -64.923	PMTOT = 56.505
T = .01257	PFI = 194.375	PMDT = 88.414	G = .0344	GDT = 12.762	PSIO = 315.113	PSINOT = -74.584	PMTOT = 56.375
T = .01267	PFI = 194.916	PMDT = 100.354	G = .0373	GDT = 14.766	PSIO = 314.618	PSINOT = -82.494	PMTOT = 56.916
T = .01277	PFI = 195.523	PMDT = 111.135	G = .0357	GDT = 16.755	PSIO = 314.049	PSINOT = -89.520	PMTOT = 60.523
T = .01287	PFI = 196.187	PMDT = 120.637	G = .0339	GDT = 18.733	PSIO = 313.508	PSINOT = -94.127	PMTOT = 61.187
T = .01297	PFI = 196.903	PMDT = 128.935	G = .0320	GDT = 20.693	PSIO = 312.996	PSINOT = -100.381	PMTOT = 61.903
T = .01307	PFI = 197.662	PMDT = 135.834	G = .0299	GDT = 21.470	PSIO = 311.915	PSINOT = -102.342	PMTOT = 62.662
T = .01317	PFI = 198.457	PMDT = 141.374	G = .0277	GDT = 23.141	PSIO = 311.066	PSINOT = -103.974	PMTOT = 61.457
T = .01327	PFI = 199.280	PMDT = 145.564	G = .0253	GDT = 24.593	PSIO = 310.151	PSINOT = -105.239	PMTOT = 60.240
T = .01337	PFI = 200.122	PMDT = 148.389	G = .0228	GDT = 25.902	PSIO = 309.173	PSINOT = -106.161	PMTOT = 65.122
T = .01347	PFI = 200.978	PMDT = 149.939	G = .0201	GDT = 27.107	PSIO = 308.134	PSINOT = -106.727	PMTOT = 65.978
T = .01357	PFI = 201.838	PMDT = 150.265	G = .0174	GDT = 28.207	PSIO = 307.036	PSINOT = -106.947	PMTOT = 66.838
T = .01367	PFI = 202.697	PMDT = 150.432	G = .0145	GDT = 29.202	PSIO = 305.883	PSINOT = -106.953	PMTOT = 67.697
T = .01377	PFI = 203.545	PMDT = 147.548	G = .0115	GDT = 30.093	PSIO = 304.677	PSINOT = -106.902	PMTOT = 68.549
T = .01387	PFI = 204.386	PMDT = 144.683	G = .0085	GDT = 30.880	PSIO = 303.422	PSINOT = -106.715	PMTOT = 69.386
T = .01397	PFI = 205.205	PMDT = 140.961	G = .0053	GDT = 31.545	PSIO = 302.119	PSINOT = -106.319	PMTOT = 70.205
T = .01407	PFI = 206.000	PMDT = 136.484	G = .0022	GDT = 32.151	PSIO = 300.774	PSINOT = -105.684	PMTOT = 71.000
T = .01417	PFI = 206.768	PMDT = 131.355	G = .0011	GDT = 32.638	PSIO = 299.388	PSINOT = -104.826	PMTOT = 71.766

## FEE MOTION

T = .01417	PFI = 196.768	PMDT = 131.355	PSI = 48.725	PSINOT = -245.226	PMTOT = 71.768
T = .01418	PFI = 196.846	PMDT = 141.766	PSI = 48.584	PSINOT = -245.226	PMTOT = 71.846
T = .01419	PFI = 196.930	PMDT = 152.178	PSI = 48.444	PSINOT = -245.226	PMTOT = 71.930
T = .01420	PFI = 197.020	PMDT = 162.590	PSI = 48.303	PSINOT = -245.226	PMTOT = 72.020
T = .01421	PFI = 197.110	PMDT = 173.002	PSI = 48.163	PSINOT = -245.226	PMTOT = 72.116
T = .01422	PFI = 197.218	PMDT = 183.414	PSI = 48.022	PSINOT = -245.226	PMTOT = 72.218
T = .01423	PFI = 197.327	PMDT = 193.825	PSI = 47.882	PSINOT = -245.226	PMTOT = 72.327
T = .01424	PFI = 197.441	PMDT = 204.237	PSI = 47.741	PSINOT = -245.226	PMTOT = 72.441
T = .01425	PFI = 197.561	PMDT = 214.649	PSI = 47.600	PSINOT = -245.226	PMTOT = 72.561
T = .01426	PFI = 197.687	PMDT = 225.061	PSI = 47.460	PSINOT = -245.226	PMTOT = 72.687
T = .01427	PFI = 197.818	PMDT = 235.472	PSI = 47.320	PSINOT = -245.226	PMTOT = 72.818
T = .01428	PFI = 197.955	PMDT = 245.884	PSI = 47.179	PSINOT = -245.226	PMTOT = 72.955
T = .01429	PFI = 198.100	PMDT = 256.296	PSI = 47.039	PSINOT = -245.226	PMTOT = 73.100
T = .01430	PFI = 198.250	PMDT = 266.708	PSI = 46.898	PSINOT = -245.226	PMTOT = 73.250
T = .01431	PFI = 198.405	PMDT = 277.119	PSI = 46.758	PSINOT = -245.226	PMTOT = 73.406
T = .01432	PFI = 198.563	PMDT = 287.531	PSI = 46.617	PSINOT = -245.226	PMTOT = 73.568
T = .01433	PFI = 198.735	PMDT = 297.943	PSI = 46.476	PSINOT = -245.226	PMTOT = 73.735
T = .01434	PFI = 198.909	PMDT = 308.355	PSI = 46.336	PSINOT = -245.226	PMTOT = 73.909
T = .01435	PFI = 199.089	PMDT = 318.766	PSI = 46.195	PSINOT = -245.226	PMTOT = 74.089
T = .01436	PFI = 199.274	PMDT = 329.178	PSI = 46.055	PSINOT = -245.226	PMTOT = 74.274
T = .01437	PFI = 199.466	PMDT = 339.590	PSI = 45.914	PSINOT = -245.226	PMTOT = 74.466
T = .01438	PFI = 199.663	PMDT = 350.002	PSI = 45.774	PSINOT = -245.226	PMTOT = 74.663
T = .01439	PFI = 199.867	PMDT = 360.414	PSI = 45.633	PSINOT = -245.226	PMTOT = 74.867
T = .01440	PFI = 200.077	PMDT = 370.825	PSI = 45.493	PSINOT = -245.226	PMTOT = 75.076
T = .01441	PFI = 200.293	PMDT = 381.237	PSI = 45.352	PSINOT = -245.226	PMTOT = 75.292
T = .01442	PFI = 200.513	PMDT = 391.649	PSI = 45.212	PSINOT = -245.226	PMTOT = 75.513
T = .01443	PFI = 200.741	PMDT = 402.061	PSI = 45.071	PSINOT = -245.226	PMTOT = 75.741

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IMPACT									
Cycle No. 3									
TE	.01445	PMI	130.974	PMDOI	412.472	PSI	42.931	PSIOOI	245.226
TE	.01445	PMI	131.213	PMDOI	422.444	PSI	42.740	PSIOOI	245.226
TE	.01446	PMI	131.450	PMDOI	433.226	PSI	44.550	PSIOOI	245.226
TE	.01447	PMI	131.710	PMDOI	441.708	PSI	44.509	PSIOOI	245.226
TE	.01448	PMI	131.967	PMDOI	454.119	PSI	44.369	PSIOOI	245.226
TE	.01449	PMI	132.230	PMDOI	466.531	PSI	44.228	PSIOOI	245.226
TE	.01450	PMI	132.499	PMDOI	474.943	PSI	44.088	PSIOOI	245.226
TE	.01451	PMI	132.774	PMDOI	485.355	PSI	43.947	PSIOOI	245.226
TE	.01452	PMI	133.056	PMDOI	495.766	PSI	43.807	PSIOOI	245.226
TE	.01453	PMI	133.343	PMDOI	506.178	PSI	43.666	PSIOOI	245.226
TE	.01454	PMI	133.636	PMDOI	516.590	PSI	43.526	PSIOOI	245.226
TE	.01455	PMI	133.935	PMDOI	527.002	PSI	43.385	PSIOOI	245.226
TE	.01456	PMI	134.239	PMDOI	537.414	PSI	43.245	PSIOOI	245.226
TE	.01457	PMI	134.550	PMDOI	547.825	PSI	43.104	PSIOOI	245.226
TE	.01458	PMI	134.867	PMDOI	558.237	PSI	42.964	PSIOOI	245.226
TE	.01459	PMI	135.190	PMDOI	568.649	PSI	42.823	PSIOOI	245.226
TE	.01460	PMI	135.519	PMDOI	579.061	PSI	42.683	PSIOOI	245.226
VP	-14.346	VS	44.940						
IMPACT									
VP	-7.234	VS	-22.056	PMI	135.519	PMDOI	234.190	PSI	42.683
FREE MOTION									
TE	.01460	PMI	135.519	PMDOI	284.190	PSI	42.683	PSIOOI	123.677
TE	.01461	PMI	135.359	PMDOI	273.779	PSI	42.612	PSIOOI	123.677
VP	-7.249	VS	-21.063						
FREE MOTION									
TE	.01461	PMI	135.359	PMDOI	273.779	PSI	42.612	PSIOOI	123.677
TE	.01462	PMI	135.205	PMDOI	263.367	PSI	42.541	PSIOOI	123.677
VP	-7.263	VS	-20.128						
FREE MOTION									
TE	.01462	PMI	135.205	PMDOI	263.367	PSI	42.541	PSIOOI	123.677
TE	.01463	PMI	135.057	PMDOI	252.955	PSI	42.470	PSIOOI	123.677
VP	-7.276	VS	-19.192						
FREE MOTION									
TE	.01463	PMI	135.057	PMDOI	252.955	PSI	42.470	PSIOOI	123.677
TE	.01464	PMI	134.915	PMDOI	242.543	PSI	42.399	PSIOOI	123.677
TE	.01465	PMI	134.779	PMDOI	232.131	PSI	42.329	PSIOOI	123.677
TE	.01466	PMI	134.649	PMDOI	221.720	PSI	42.258	PSIOOI	123.677
TE	.01467	PMI	134.525	PMDOI	211.308	PSI	42.187	PSIOOI	123.677
TE	.01468	PMI	134.407	PMDOI	200.896	PSI	42.116	PSIOOI	123.677
TE	.01469	PMI	134.295	PMDOI	190.484	PSI	42.045	PSIOOI	123.677
TE	.01470	PMI	134.189	PMDOI	180.073	PSI	41.974	PSIOOI	123.677
TE	.01471	PMI	134.089	PMDOI	169.661	PSI	41.903	PSIOOI	123.677
TE	.01472	PMI	133.994	PMDOI	159.249	PSI	41.833	PSIOOI	123.677
TE	.01473	PMI	133.906	PMDOI	148.837	PSI	41.762	PSIOOI	123.677
TE	.01474	PMI	133.824	PMDOI	138.426	PSI	41.691	PSIOOI	123.677
TE	.01475	PMI	133.748	PMDOI	128.014	PSI	41.620	PSIOOI	123.677
TE	.01476	PMI	133.677	PMDOI	117.602	PSI	41.549	PSIOOI	123.677
TE	.01477	PMI	133.613	PMDOI	107.190	PSI	41.478	PSIOOI	123.677
TE	.01478	PMI	133.556	PMDOI	96.779	PSI	41.407	PSIOOI	123.677
TE	.01479	PMI	133.502	PMDOI	86.367	PSI	41.337	PSIOOI	123.677
TE	.01480	PMI	133.455	PMDOI	75.955	PSI	41.266	PSIOOI	123.677
TE	.01481	PMI	133.415	PMDOI	65.543	PSI	41.195	PSIOOI	123.677
TE	.01482	PMI	133.380	PMDOI	55.131	PSI	41.124	PSIOOI	123.677
TE	.01483	PMI	133.352	PMDOI	44.720	PSI	41.053	PSIOOI	123.677
TE	.01484	PMI	133.329	PMDOI	34.308	PSI	40.982	PSIOOI	123.677
TE	.01485	PMI	133.312	PMDOI	23.896	PSI	40.911	PSIOOI	123.677
TE	.01486	PMI	133.302	PMDOI	13.484	PSI	40.840	PSIOOI	123.677
TE	.01487	PMI	133.297	PMDOI	3.073	PSI	40.770	PSIOOI	123.677
TE	.01488	PMI	133.298	PMDOI	7.339	PSI	40.699	PSIOOI	123.677

1	05256	PHI = 202.414	PHIDOT = 152.345	G = -0.0154	GDOT = 30.371	PSI001 = 246.454	PHITOT = 271.571	PSI001 = 246.454	PHI001 = 271.571
2	05266	PHI = 203.282	PHIDOT = 150.537	G = -0.0125	GDOT = 30.286	PSI001 = 246.454	PHITOT = 271.651	PSI001 = 246.454	PHI001 = 271.651
3	05276	PHI = 204.137	PHIDOT = 147.725	G = -0.0094	GDOT = 31.096	PSI001 = 246.454	PHITOT = 271.737	PSI001 = 246.454	PHI001 = 271.737
4	05286	PHI = 204.973	PHIDOT = 144.015	G = -0.0062	GDOT = 31.802	PSI001 = 246.454	PHITOT = 271.829	PSI001 = 246.454	PHI001 = 271.829
5	05296	PHI = 205.786	PHIDOT = 139.514	G = -0.0030	GDOT = 32.407	PSI001 = 246.454	PHITOT = 271.927	PSI001 = 246.454	PHI001 = 271.927
6	05306	PHI = 206.571	PHIDOT = 134.339	G = -0.0002	GDOT = 32.912	PSI001 = 246.454	PHITOT = 272.030	PSI001 = 246.454	PHI001 = 272.030
FREE MOTION									
7	05306	PHI = 126.571	PHIDOT = 134.339	PSI = 49.088	PSIDOT = 246.454	PHITOT = 271.571	PSI001 = 246.454	PHITOT = 271.571	PSI001 = 246.454
8	05307	PHI = 126.651	PHIDOT = 144.751	PSI = 48.947	PSIDOT = 246.454	PHITOT = 271.651	PSI001 = 246.454	PHITOT = 271.651	PSI001 = 246.454
9	05308	PHI = 126.737	PHIDOT = 155.163	PSI = 48.806	PSIDOT = 246.454	PHITOT = 271.737	PSI001 = 246.454	PHITOT = 271.737	PSI001 = 246.454
10	05309	PHI = 126.829	PHIDOT = 165.574	PSI = 48.665	PSIDOT = 246.454	PHITOT = 271.829	PSI001 = 246.454	PHITOT = 271.829	PSI001 = 246.454
11	05310	PHI = 126.927	PHIDOT = 175.986	PSI = 48.524	PSIDOT = 246.454	PHITOT = 271.927	PSI001 = 246.454	PHITOT = 271.927	PSI001 = 246.454
12	05311	PHI = 127.030	PHIDOT = 186.398	PSI = 48.382	PSIDOT = 246.454	PHITOT = 272.030	PSI001 = 246.454	PHITOT = 272.030	PSI001 = 246.454
13	05312	PHI = 127.140	PHIDOT = 196.810	PSI = 48.241	PSIDOT = 246.454	PHITOT = 272.140	PSI001 = 246.454	PHITOT = 272.140	PSI001 = 246.454
14	05313	PHI = 127.256	PHIDOT = 207.221	PSI = 48.100	PSIDOT = 246.454	PHITOT = 272.256	PSI001 = 246.454	PHITOT = 272.256	PSI001 = 246.454
15	05314	PHI = 127.378	PHIDOT = 217.633	PSI = 47.959	PSIDOT = 246.454	PHITOT = 272.378	PSI001 = 246.454	PHITOT = 272.378	PSI001 = 246.454
16	05315	PHI = 127.505	PHIDOT = 228.045	PSI = 47.818	PSIDOT = 246.454	PHITOT = 272.505	PSI001 = 246.454	PHITOT = 272.505	PSI001 = 246.454
17	05316	PHI = 127.639	PHIDOT = 238.457	PSI = 47.676	PSIDOT = 246.454	PHITOT = 272.639	PSI001 = 246.454	PHITOT = 272.639	PSI001 = 246.454
18	05317	PHI = 127.779	PHIDOT = 248.868	PSI = 47.535	PSIDOT = 246.454	PHITOT = 272.779	PSI001 = 246.454	PHITOT = 272.779	PSI001 = 246.454
19	05318	PHI = 127.924	PHIDOT = 259.280	PSI = 47.394	PSIDOT = 246.454	PHITOT = 272.924	PSI001 = 246.454	PHITOT = 272.924	PSI001 = 246.454
20	05319	PHI = 128.074	PHIDOT = 269.692	PSI = 47.253	PSIDOT = 246.454	PHITOT = 273.076	PSI001 = 246.454	PHITOT = 273.076	PSI001 = 246.454
21	05320	PHI = 128.231	PHIDOT = 280.104	PSI = 47.112	PSIDOT = 246.454	PHITOT = 273.233	PSI001 = 246.454	PHITOT = 273.233	PSI001 = 246.454
22	05321	PHI = 128.397	PHIDOT = 290.515	PSI = 46.970	PSIDOT = 246.454	PHITOT = 273.397	PSI001 = 246.454	PHITOT = 273.397	PSI001 = 246.454
23	05322	PHI = 128.566	PHIDOT = 300.927	PSI = 46.829	PSIDOT = 246.454	PHITOT = 273.566	PSI001 = 246.454	PHITOT = 273.566	PSI001 = 246.454
24	05323	PHI = 128.741	PHIDOT = 311.339	PSI = 46.688	PSIDOT = 246.454	PHITOT = 273.741	PSI001 = 246.454	PHITOT = 273.741	PSI001 = 246.454
25	05324	PHI = 128.923	PHIDOT = 321.751	PSI = 46.547	PSIDOT = 246.454	PHITOT = 273.923	PSI001 = 246.454	PHITOT = 273.923	PSI001 = 246.454
26	05325	PHI = 129.110	PHIDOT = 332.163	PSI = 46.406	PSIDOT = 246.454	PHITOT = 274.110	PSI001 = 246.454	PHITOT = 274.110	PSI001 = 246.454
27	05326	PHI = 129.303	PHIDOT = 342.574	PSI = 46.264	PSIDOT = 246.454	PHITOT = 274.303	PSI001 = 246.454	PHITOT = 274.303	PSI001 = 246.454
28	05327	PHI = 129.503	PHIDOT = 352.986	PSI = 46.123	PSIDOT = 246.454	PHITOT = 274.503	PSI001 = 246.454	PHITOT = 274.503	PSI001 = 246.454
29	05328	PHI = 129.708	PHIDOT = 363.398	PSI = 45.982	PSIDOT = 246.454	PHITOT = 274.708	PSI001 = 246.454	PHITOT = 274.708	PSI001 = 246.454
30	05329	PHI = 129.919	PHIDOT = 373.810	PSI = 45.841	PSIDOT = 246.454	PHITOT = 274.919	PSI001 = 246.454	PHITOT = 274.919	PSI001 = 246.454
31	05330	PHI = 130.136	PHIDOT = 384.221	PSI = 45.699	PSIDOT = 246.454	PHITOT = 275.136	PSI001 = 246.454	PHITOT = 275.136	PSI001 = 246.454
32	05331	PHI = 130.359	PHIDOT = 394.633	PSI = 45.558	PSIDOT = 246.454	PHITOT = 275.359	PSI001 = 246.454	PHITOT = 275.359	PSI001 = 246.454
33	05332	PHI = 130.588	PHIDOT = 405.045	PSI = 45.417	PSIDOT = 246.454	PHITOT = 275.588	PSI001 = 246.454	PHITOT = 275.588	PSI001 = 246.454
34	05333	PHI = 130.824	PHIDOT = 415.457	PSI = 45.276	PSIDOT = 246.454	PHITOT = 275.824	PSI001 = 246.454	PHITOT = 275.824	PSI001 = 246.454
35	05334	PHI = 131.065	PHIDOT = 425.868	PSI = 45.135	PSIDOT = 246.454	PHITOT = 276.065	PSI001 = 246.454	PHITOT = 276.065	PSI001 = 246.454
36	05335	PHI = 131.312	PHIDOT = 436.280	PSI = 44.993	PSIDOT = 246.454	PHITOT = 276.312	PSI001 = 246.454	PHITOT = 276.312	PSI001 = 246.454
37	05336	PHI = 131.565	PHIDOT = 446.692	PSI = 44.852	PSIDOT = 246.454	PHITOT = 276.565	PSI001 = 246.454	PHITOT = 276.565	PSI001 = 246.454
38	05337	PHI = 131.823	PHIDOT = 457.104	PSI = 44.711	PSIDOT = 246.454	PHITOT = 276.823	PSI001 = 246.454	PHITOT = 276.823	PSI001 = 246.454
39	05338	PHI = 132.088	PHIDOT = 467.515	PSI = 44.570	PSIDOT = 246.454	PHITOT = 277.088	PSI001 = 246.454	PHITOT = 277.088	PSI001 = 246.454
40	05339	PHI = 132.359	PHIDOT = 477.927	PSI = 44.429	PSIDOT = 246.454	PHITOT = 277.359	PSI001 = 246.454	PHITOT = 277.359	PSI001 = 246.454
41	05340	PHI = 132.636	PHIDOT = 488.339	PSI = 44.287	PSIDOT = 246.454	PHITOT = 277.636	PSI001 = 246.454	PHITOT = 277.636	PSI001 = 246.454
42	05341	PHI = 132.919	PHIDOT = 498.751	PSI = 44.146	PSIDOT = 246.454	PHITOT = 277.919	PSI001 = 246.454	PHITOT = 277.919	PSI001 = 246.454
43	05342	PHI = 133.208	PHIDOT = 509.163	PSI = 44.005	PSIDOT = 246.454	PHITOT = 278.208	PSI001 = 246.454	PHITOT = 278.208	PSI001 = 246.454
44	05343	PHI = 133.502	PHIDOT = 519.574	PSI = 43.864	PSIDOT = 246.454	PHITOT = 278.502	PSI001 = 246.454	PHITOT = 278.502	PSI001 = 246.454
45	05344	PHI = 133.803	PHIDOT = 529.986	PSI = 43.723	PSIDOT = 246.454	PHITOT = 278.803	PSI001 = 246.454	PHITOT = 278.803	PSI001 = 246.454
46	05345	PHI = 134.110	PHIDOT = 540.398	PSI = 43.581	PSIDOT = 246.454	PHITOT = 279.110	PSI001 = 246.454	PHITOT = 279.110	PSI001 = 246.454
47	05346	PHI = 134.422	PHIDOT = 550.810	PSI = 43.440	PSIDOT = 246.454	PHITOT = 279.422	PSI001 = 246.454	PHITOT = 279.422	PSI001 = 246.454
48	05347	PHI = 134.741	PHIDOT = 561.221	PSI = 43.299	PSIDOT = 246.454	PHITOT = 279.741	PSI001 = 246.454	PHITOT = 279.741	PSI001 = 246.454
49	05348	PHI = 135.065	PHIDOT = 571.633	PSI = 43.158	PSIDOT = 246.454	PHITOT = 280.065	PSI001 = 246.454	PHITOT = 280.065	PSI001 = 246.454
50	05349	PHI = 135.386	PHIDOT = 582.045	PSI = 43.017	PSIDOT = 246.454	PHITOT = 280.386	PSI001 = 246.454	PHITOT = 280.386	PSI001 = 246.454
51	05350	PHI = 135.732	PHIDOT = 592.457	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
VP = 14.489 VS = 46.458									
IMPACT									
Cycle No. 8									
52	05351	PHI = 135.732	DPHIF = 286.525	PSI = 42.875	DPSEIF = 124.023	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
53	05352	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
54	05353	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
55	05354	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
56	05355	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
57	05356	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
58	05357	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
59	05358	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
60	05359	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
61	05360	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
62	05361	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
63	05362	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
64	05363	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
65	05364	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
66	05365	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732	PSI001 = 246.454	PHITOT = 280.732	PSI001 = 246.454
67	05366	PHI = 135.732	PHIDOT = 286.525	PSI = 42.875	PSIDOT = 246.454	PHITOT = 280.732			

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FREE MOTION									
T=	.05351	PHI= 135.571	PHOOT=276.113	PSI= 42.896	PSINOT=-124.023	PHITOT = 280.571			
T=	.05352	PHI= 135.416	PHOOT=265.701	PSI= 42.733	PSINOT=-124.023	PHITOT = 280.416			
VP=	-7.280	VS= -20.517							
FREE MOTION									
T=	.05352	PHI= 135.416	PHOOT=265.701	PSI= 42.733	PSINOT=-124.023	PHITOT = 280.416			
T=	.05353	PHI= 135.267	PHOOT=255.289	PSI= 42.662	PSINOT=-124.023	PHITOT = 280.267			
VP=	-7.293	VS= -19.570							
FREE MOTION									
T=	.05353	PHI= 135.267	PHOOT=255.289	PSI= 42.662	PSINOT=-124.023	PHITOT = 280.267			
T=	.05354	PHI= 134.878	PHOOT=244.878	PSI= 42.591	PSINOT=-124.023	PHITOT = 280.123			
T=	.05355	PHI= 134.946	PHOOT=234.466	PSI= 42.520	PSINOT=-124.023	PHITOT = 279.986			
T=	.05356	PHI= 134.855	PHOOT=224.054	PSI= 42.449	PSINOT=-124.023	PHITOT = 279.855			
T=	.05357	PHI= 134.729	PHOOT=213.642	PSI= 42.378	PSINOT=-124.023	PHITOT = 279.729			
T=	.05358	PHI= 134.610	PHOOT=203.231	PSI= 42.307	PSINOT=-124.023	PHITOT = 279.610			
T=	.05359	PHI= 134.496	PHOOT=192.819	PSI= 42.236	PSINOT=-124.023	PHITOT = 279.496			
FREE MOTION									
T=	.05360	PHI= 134.389	PHOOT=182.407	PSI= 42.165	PSINOT=-124.023	PHITOT = 279.389			
T=	.05361	PHI= 134.287	PHOOT=171.995	PSI= 42.094	PSINOT=-124.023	PHITOT = 279.287			
T=	.05362	PHI= 134.192	PHOOT=161.583	PSI= 42.023	PSINOT=-124.023	PHITOT = 279.192			
T=	.05363	PHI= 134.102	PHOOT=151.172	PSI= 41.952	PSINOT=-124.023	PHITOT = 279.102			
T=	.05364	PHI= 134.019	PHOOT=140.760	PSI= 41.880	PSINOT=-124.023	PHITOT = 279.019			
T=	.05365	PHI= 133.941	PHOOT=130.348	PSI= 41.809	PSINOT=-124.023	PHITOT = 278.941			
T=	.05366	PHI= 133.869	PHOOT=119.936	PSI= 41.738	PSINOT=-124.023	PHITOT = 278.869			
T=	.05367	PHI= 133.803	PHOOT=109.525	PSI= 41.667	PSINOT=-124.023	PHITOT = 278.803			
T=	.05368	PHI= 133.744	PHOOT=99.113	PSI= 41.596	PSINOT=-124.023	PHITOT = 278.744			
T=	.05369	PHI= 133.690	PHOOT=88.701	PSI= 41.525	PSINOT=-124.023	PHITOT = 278.690			
T=	.05370	PHI= 133.642	PHOOT=78.289	PSI= 41.454	PSINOT=-124.023	PHITOT = 278.642			
T=	.05371	PHI= 133.600	PHOOT=67.878	PSI= 41.383	PSINOT=-124.023	PHITOT = 278.600			
T=	.05372	PHI= 133.564	PHOOT=57.466	PSI= 41.312	PSINOT=-124.023	PHITOT = 278.564			
T=	.05373	PHI= 133.534	PHOOT=47.054	PSI= 41.241	PSINOT=-124.023	PHITOT = 278.534			
T=	.05374	PHI= 133.510	PHOOT=36.642	PSI= 41.170	PSINOT=-124.023	PHITOT = 278.510			
T=	.05375	PHI= 133.492	PHOOT=26.231	PSI= 41.099	PSINOT=-124.023	PHITOT = 278.492			
T=	.05376	PHI= 133.480	PHOOT=15.819	PSI= 41.028	PSINOT=-124.023	PHITOT = 278.480			
T=	.05377	PHI= 133.474	PHOOT=5.407	PSI= 40.957	PSINOT=-124.023	PHITOT = 278.474			
T=	.05378	PHI= 133.474	PHOOT=5.005	PSI= 40.886	PSINOT=-124.023	PHITOT = 278.474			
T=	.05379	PHI= 133.480	PHOOT=15.617	PSI= 40.815	PSINOT=-124.023	PHITOT = 278.480			
T=	.05380	PHI= 133.492	PHOOT=25.828	PSI= 40.744	PSINOT=-124.023	PHITOT = 278.492			
T=	.05381	PHI= 133.509	PHOOT=36.240	PSI= 40.672	PSINOT=-124.023	PHITOT = 278.509			
T=	.05382	PHI= 133.533	PHOOT=46.652	PSI= 40.601	PSINOT=-124.023	PHITOT = 278.533			
T=	.05383	PHI= 133.563	PHOOT=57.064	PSI= 40.530	PSINOT=-124.023	PHITOT = 278.563			
VP=	-7.222	VS= 4.015							
IMPACT									
VP=	-5.629	VS= -8.437							
FREE MOTION									
T=	.05383	PHI= 133.563	PHOOT=119.929	PSI= 40.530	PSINOT=-96.656	PHITOT = 278.563			
T=	.05384	PHI= 133.497	PHOOT=109.517	PSI= 40.459	PSINOT=-96.656	PHITOT = 278.497			
VP=	-5.630	VS= -7.679							
FREE MOTION									
T=	.05384	PHI= 133.497	PHOOT=109.517	PSI= 40.475	PSINOT=-96.656	PHITOT = 278.497			
T=	.05385	PHI= 133.437	PHOOT=99.105	PSI= 40.420	PSINOT=-96.656	PHITOT = 278.437			
VP=	-5.630	VS= -6.927							
FREE MOTION									
T=	.05385	PHI= 133.437	PHOOT=99.105	PSI= 40.420	PSINOT=-96.656	PHITOT = 278.437			
T=	.05386	PHI= 133.384	PHOOT=88.694	PSI= 40.364	PSINOT=-96.656	PHITOT = 278.384			
VP=	-5.630	VS= -6.182							

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NO: 104 3383

--	1E	0.05387	PMI	133.336	PMDOI	-78.282	PSI	40.309	PSDOI	-96.656	PMIOT	278.336
--	1E	0.05386	PMI	133.384	PMDOI	-88.694	PSI	40.364	PSDOI	-96.656	PMIOT	278.384

6275-5.629

**Capacity**

$\rho_{H_2O} = 133.336$      $\rho_{H_2O} = -0.242$      $\rho_{Si} = 40.309$      $\rho_{SiF_6} = -96.193$      $\rho_{H_2OT} = 278.33K$

"COVER STORY"

[illegible]

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T	.05627	PHI = 178.206	PHI001 = 81.781	G = -.0333	GO01 = 18.454	PSID = 46.413	PSID001 = 119.092	PHI01 = 253.208
T	.05637	PHI = 178.642	PHI001 = 86.094	G = -.0315	GO01 = 19.009	PSID = 47.510	PSID001 = 120.473	PHI01 = 283.582
T	.05647	PHI = 179.170	PHI001 = 86.312	G = -.0295	GO01 = 19.726	PSID = 48.239	PSID001 = 120.835	PHI01 = 284.170
T	.05657	PHI = 179.671	PHI001 = 86.436	G = -.0275	GO01 = 20.315	PSID = 48.998	PSID001 = 125.178	PHI01 = 284.671
T	.05667	PHI = 180.183	PHI001 = 90.471	G = -.0255	GO01 = 20.927	PSID = 49.748	PSID001 = 140.566	PHI01 = 285.143
T	.05677	PHI = 180.707	PHI001 = 92.412	G = -.0233	GO01 = 21.504	PSID = 50.604	PSID001 = 145.819	PHI01 = 285.707
T	.05687	PHI = 181.242	PHI001 = 94.325	G = -.0212	GO01 = 22.044	PSID = 51.450	PSID001 = 151.121	PHI01 = 286.242
T	.05697	PHI = 181.788	PHI001 = 96.154	G = -.0199	GO01 = 22.610	PSID = 52.340	PSID001 = 156.414	PHI01 = 286.788
T	.05707	PHI = 182.344	PHI001 = 97.934	G = -.0184	GO01 = 23.141	PSID = 53.251	PSID001 = 161.700	PHI01 = 287.344
T	.05717	PHI = 182.910	PHI001 = 99.672	G = -.0163	GO01 = 23.658	PSID = 54.193	PSID001 = 166.980	PHI01 = 287.910
T	.05727	PHI = 183.486	PHI001 = 101.364	G = -.0139	GO01 = 24.141	PSID = 55.165	PSID001 = 172.254	PHI01 = 288.486
T	.05737	PHI = 184.072	PHI001 = 103.022	G = -.0119	GO01 = 24.651	PSID = 56.167	PSID001 = 177.536	PHI01 = 289.072
T	.05747	PHI = 184.667	PHI001 = 104.650	G = -.0097	GO01 = 25.127	PSID = 57.199	PSID001 = 182.816	PHI01 = 289.667
T	.05757	PHI = 185.271	PHI001 = 106.252	G = -.0074	GO01 = 25.590	PSID = 58.262	PSID001 = 188.094	PHI01 = 290.271
T	.05767	PHI = 185.884	PHI001 = 107.834	G = -.0051	GO01 = 26.040	PSID = 59.355	PSID001 = 193.387	PHI01 = 290.884
T	.05777	PHI = 186.505	PHI001 = 109.402	G = -.0028	GO01 = 26.477	PSID = 60.478	PSID001 = 198.683	PHI01 = 291.506
PAGE BOTTOM								
T	.05777	PHI = 186.506	PH001 = 109.402	PSI = 311.141	PSID001 = 198.683	PHI01 = 291.506		
T	.05778	PHI = 186.572	PH001 = 119.814	PSI = 311.255	PSID001 = 198.683	PHI01 = 291.572		
T	.05779	PHI = 186.644	PH001 = 130.226	PSI = 311.368	PSID001 = 198.683	PHI01 = 291.644		
T	.05780	PHI = 186.721	PH001 = 140.638	PSI = 311.482	PSID001 = 198.683	PHI01 = 291.721		
T	.05781	PHI = 186.805	PH001 = 151.049	PSI = 311.594	PSID001 = 198.683	PHI01 = 291.805		
T	.05782	PHI = 186.894	PH001 = 161.461	PSI = 311.710	PSID001 = 198.683	PHI01 = 291.894		
T	.05783	PHI = 186.990	PH001 = 171.873	PSI = 311.824	PSID001 = 198.683	PHI01 = 291.920		
T	.05784	PHI = 187.091	PH001 = 182.285	PSI = 311.938	PSID001 = 198.683	PHI01 = 292.001		
T	.05785	PHI = 187.199	PH001 = 192.696	PSI = 312.051	PSID001 = 198.683	PHI01 = 292.199		
T	.05786	PHI = 187.312	PH001 = 203.108	PSI = 312.165	PSID001 = 198.683	PHI01 = 292.312		
T	.05787	PHI = 187.432	PH001 = 213.520	PSI = 312.279	PSID001 = 198.683	PHI01 = 292.432		
T	.05788	PHI = 187.557	PH001 = 223.932	PSI = 312.393	PSID001 = 198.683	PHI01 = 292.557		
T	.05789	PHI = 187.684	PH001 = 234.343	PSI = 312.507	PSID001 = 198.683	PHI01 = 292.684		
T	.05790	PHI = 187.825	PH001 = 244.755	PSI = 312.621	PSID001 = 198.683	PHI01 = 292.825		
T	.05791	PHI = 187.965	PH001 = 255.167	PSI = 312.734	PSID001 = 198.683	PHI01 = 292.969		
T	.05792	PHI = 188.118	PH001 = 265.579	PSI = 312.848	PSID001 = 198.683	PHI01 = 293.118		
T	.05793	PHI = 188.273	PH001 = 275.990	PSI = 312.962	PSID001 = 198.683	PHI01 = 293.273		
T	.05794	PHI = 188.434	PH001 = 286.402	PSI = 313.076	PSID001 = 198.683	PHI01 = 293.434		
T	.05795	PHI = 188.601	PH001 = 296.814	PSI = 313.190	PSID001 = 198.683	PHI01 = 293.601		
T	.05796	PHI = 188.774	PH001 = 307.226	PSI = 313.304	PSID001 = 198.683	PHI01 = 293.774		
T	.05797	PHI = 188.953	PH001 = 317.638	PSI = 313.417	PSID001 = 198.683	PHI01 = 293.953		
T	.05798	PHI = 189.138	PH001 = 328.049	PSI = 313.531	PSID001 = 198.683	PHI01 = 294.138		
T	.05799	PHI = 189.329	PH001 = 338.461	PSI = 313.645	PSID001 = 198.683	PHI01 = 294.329		
T	.05800	PHI = 189.526	PH001 = 348.873	PSI = 313.759	PSID001 = 198.683	PHI01 = 294.526		
T	.05801	PHI = 189.729	PH001 = 359.285	PSI = 313.873	PSID001 = 198.683	PHI01 = 294.729		
T	.05802	PHI = 189.938	PH001 = 369.696	PSI = 313.987	PSID001 = 198.683	PHI01 = 294.938		
T	.05803	PHI = 190.153	PH001 = 380.108	PSI = 314.101	PSID001 = 198.683	PHI01 = 295.153		
T	.05804	PHI = 190.373	PH001 = 390.520	PSI = 314.214	PSID001 = 198.683	PHI01 = 295.373		
T	.05805	PHI = 190.600	PH001 = 400.932	PSI = 314.328	PSID001 = 198.683	PHI01 = 295.600		
T	.05806	PHI = 190.833	PH001 = 411.343	PSI = 314.442	PSID001 = 198.683	PHI01 = 295.833		
T	.05807	PHI = 191.071	PH001 = 421.755	PSI = 314.556	PSID001 = 198.683	PHI01 = 296.071		
T	.05808	PHI = 191.316	PH001 = 432.167	PSI = 314.670	PSID001 = 198.683	PHI01 = 296.316		
T	.05809	PHI = 191.567	PH001 = 442.579	PSI = 314.784	PSID001 = 198.683	PHI01 = 296.567		
T	.05810	PHI = 191.823	PH001 = 452.990	PSI = 314.897	PSID001 = 198.683	PHI01 = 296.823		
T	.05811	PHI = 192.086	PH001 = 463.402	PSI = 315.011	PSID001 = 198.683	PHI01 = 297.086		
T	.05812	PHI = 192.356	PH001 = 473.814	PSI = 315.125	PSID001 = 198.683	PHI01 = 297.354		
T	.05813	PHI = 192.629	PH001 = 484.226	PSI = 315.239	PSID001 = 198.683	PHI01 = 297.629		
T	.05814	PHI = 192.909	PH001 = 494.638	PSI = 315.353	PSID001 = 198.683	PHI01 = 297.909		
T	.05815	PHI = 193.196	PH001 = 505.049	PSI = 315.467	PSID001 = 198.683	PHI01 = 298.196		
T	.05816	PHI = 193.488	PH001 = 515.461	PSI = 315.580	PSID001 = 198.683	PHI01 = 298.488		
T	.05817	PHI = 193.786	PH001 = 525.873	PSI = 315.694	PSID001 = 198.683	PHI01 = 298.786		
VD = -18.247 VS = 42.715								
IMPACT								
T	.05818	PHI = 193.786	DPHIF = 231.270	PSI = 315.694	NP5IF = 38.403	PHI01 = 298.786		





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VP= -16.417 VS= 43.578

IMPACT

VP= -7.311 VS= -21.864

FREE MOTION

VP= -7.325 VS= -20.845

FREE MOTION

VP= -7.319 VS= -19.901

FREE MOTION

VP= -7.311 VS= -21.864

IMPACT

VP= -7.311 VS= -21.864

FREE MOTION

VP= -7.325 VS= -20.845

FREE MOTION

VP= -7.319 VS= -19.901

FREE MOTION

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IMPACT  
T= .06149 P=133.955 P=DOF= 17.971 P=1= 40.457 P=DOF= -124.799 P=DOF= 314.095  
T= .06150 P=133.108 P=DOF= 28.282 P=1= 40.384 P=DOF= -124.799 P=DOF= 318.108  
T= .06151 P=133.127 P=DOF= 38.794 P=1= 40.314 P=DOF= -124.799 P=DOF= 318.127  
T= .06152 P=133.152 P=DOF= 49.206 P=1= 40.243 P=DOF= -124.799 P=DOF= 318.152  
T= .06153 P=133.166 P=DOF= 59.618 P=1= 40.171 P=DOF= -124.799 P=DOF= 318.166  
T= .06154 P=133.221 P=DOF= 70.029 P=1= 40.100 P=DOF= -124.799 P=DOF= 318.221  
V= -7.752 VS= 4.840

IMPACT  
T= .06149 P=133.221 P=DOF= -123.159 P=1= 40.100 P=DOF= -94.453 P=DOF= 318.221  
V= -5.609 VS= -8.517

FREE MOTION  
T= .06154 P=133.221 P=DOF= -123.159 P=1= 40.100 P=DOF= -94.453 P=DOF= 318.221  
T= .06155 P=133.153 P=DOF= -112.747 P=1= 40.046 P=DOF= -94.453 P=DOF= 318.153  
V= -5.400 VS= -7.765

FREE MOTION  
T= .06155 P=133.153 P=DOF= -112.747 P=1= 40.046 P=DOF= -94.453 P=DOF= 318.153  
T= .06156 P=133.092 P=DOF= -102.336 P=1= 39.992 P=DOF= -94.453 P=DOF= 318.092  
V= -5.401 VS= -7.025

FREE MOTION  
T= .06156 P=133.092 P=DOF= -102.336 P=1= 39.992 P=DOF= -94.453 P=DOF= 318.092  
T= .06157 P=133.036 P=DOF= -91.924 P=1= 39.937 P=DOF= -94.453 P=DOF= 318.036  
V= -5.402 VS= -6.202

FREE MOTION  
T= .06157 P=133.036 P=DOF= -91.924 P=1= 39.937 P=DOF= -94.453 P=DOF= 318.036  
T= .06158 P=132.986 P=DOF= -81.512 P=1= 39.883 P=DOF= -94.453 P=DOF= 317.986  
V= -5.401 VS= -5.564

FREE MOTION  
T= .06158 P=132.986 P=DOF= -81.512 P=1= 39.883 P=DOF= -94.453 P=DOF= 317.986  
T= .06159 P=132.943 P=DOF= -71.106 P=1= 39.829 P=DOF= -94.453 P=DOF= 317.943  
V= -5.400 VS= -4.867

IMPACT  
T= .06159 P=132.943 P=DOF= -81.556 P=1= 39.829 P=DOF= -92.786 P=DOF= 317.943  
V= -5.363 VS= -5.555

APPENDIX J

COMPUTER OUTPUT FOR STANDARD CONFIGURATION  
WITH  $\mu = .3$  AND  $\varepsilon = 0$

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Appendix J  
Std. Config.  
μ = .5, ε = 0

A = .19310 R = .15838 C = .09683 R = .01365 ALPHA = 40.0000

TORQUE = .17760E-01 COFR = .30000E+00 IPAL = .01000E-07 ISTAR = .17000E-07

EREST = 0.00 LAMBDA = 109.337 DELTA = 40.000

Cycle No. 1

COUPLED MOTION		FREE MOTION	
T = 0.00000	PMI = 135.000	PHINT = 0.000	G = 0.000
T = 0.00000	PMI = 135.000	PHINT = 0.042	G = 0.057
T = 0.00000	PMI = 135.030	PHINT = 0.151	G = 0.057
T = 0.00000	PMI = 135.000	PHINT = 0.219	G = 0.057
T = 0.00001	PMI = 135.000	PHINT = 0.284	G = 0.057
T = 0.00001	PMI = 135.000	PHINT = 0.421	G = 0.057
T = 0.00001	PMI = 135.000	PHINT = 0.554	G = 0.057
T = 0.00002	PMI = 135.000	PHINT = 0.827	G = 0.057
T = 0.00002	PMI = 135.001	PHINT = 1.097	G = 0.057
T = 0.00004	PMI = 135.002	PHINT = 1.637	G = 0.057
T = 0.00005	PMI = 135.003	PHINT = 2.177	G = 0.057
T = 0.00007	PMI = 135.007	PHINT = 3.254	G = 0.056
T = 0.00010	PMI = 135.012	PHINT = 4.335	G = 0.056
T = 0.00015	PMI = 135.028	PHINT = 6.490	G = 0.056
T = 0.00020	PMI = 135.050	PHINT = 8.639	G = 0.055
T = 0.00030	PMI = 135.111	PHINT = 12.917	G = 0.053
T = 0.00040	PMI = 135.198	PHINT = 17.142	G = 0.049
T = 0.00050	PMI = 135.308	PHINT = 21.317	G = 0.045
T = 0.00060	PMI = 135.442	PHINT = 25.471	G = 0.040
T = 0.00070	PMI = 135.599	PHINT = 29.474	G = 0.036
T = 0.00080	PMI = 135.779	PHINT = 33.368	G = 0.027
T = 0.00090	PMI = 135.981	PHINT = 37.180	G = 0.020
T = 0.00100	PMI = 136.205	PHINT = 40.911	G = 0.011
T = 0.00110	PMI = 136.443	PHINT = 44.522	G = 0.002
T = 0.00120	PMI = 136.715	PHINT = 48.014	G = 0.002
T = 0.00130	PMI = 136.999	PHINT = 51.397	G = 0.001
T = 0.00140	PMI = 137.303	PHINT = 54.659	G = 0.000
T = 0.00150	PMI = 137.628	PHINT = 57.804	G = 0.000
T = 0.00160	PMI = 137.966	PHINT = 60.831	G = 0.000
T = 0.00170	PMI = 138.322	PHINT = 63.758	G = 0.000
T = 0.00180	PMI = 138.696	PHINT = 66.554	G = 0.000
T = 0.00190	PMI = 139.085	PHINT = 69.261	G = 0.000
T = 0.00200	PMI = 139.489	PHINT = 71.884	G = 0.000
T = 0.00210	PMI = 139.908	PHINT = 74.372	G = 0.000
T = 0.00220	PMI = 140.341	PHINT = 76.798	G = 0.000
T = 0.00230	PMI = 140.788	PHINT = 79.125	G = 0.000
T = 0.00240	PMI = 141.248	PHINT = 81.381	G = 0.000
T = 0.00250	PMI = 141.721	PHINT = 83.564	G = 0.000
T = 0.00260	PMI = 142.205	PHINT = 85.687	G = 0.000
T = 0.00270	PMI = 142.702	PHINT = 87.749	G = 0.000
T = 0.00280	PMI = 143.211	PHINT = 89.741	G = 0.000
T = 0.00290	PMI = 143.731	PHINT = 91.692	G = 0.000
T = 0.00300	PMI = 144.261	PHINT = 93.594	G = 0.000
T = 0.00310	PMI = 144.803	PHINT = 95.457	G = 0.000
T = 0.00320	PMI = 145.355	PHINT = 97.292	G = 0.000
T = 0.00330	PMI = 145.918	PHINT = 99.090	G = 0.000
T = 0.00340	PMI = 146.491	PHINT = 100.859	G = 0.000

FROM COPY Furnished by WFO

**COUPLED MOTION**

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Y=	.00404	PMI=	193.776	PM100T=	.962	G=	-.0401	GD01=	.122	PS10=	315.668	PS100T=	-.780	PM101=	194.776
T=	.00405	PMI=	193.776	PM100T=	1.092	G=	-.0401	GD01=	.145	PS10=	315.668	PS100T=	-.964	PM101=	194.776
T=	.00405	PMI=	193.776	PM100T=	1.557	G=	-.0401	GD01=	.221	PS10=	315.668	PS100T=	-1.2370	PM101=	194.776
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T= .00801 PM1= 179.754 PMDOT= 1989.994 PSI= 24.504 PSINOT= -236.225 PM1101= 84.754  
T= .00802 PM1= 180.080 PMDOT= 1999.406 PSI= 24.369 PSINOT= -236.225 PM1101= 85.080  
T= .00803 PM1= 180.406 PMDOT= 2009.818 PSI= 24.234 PSINOT= -236.225 PM1101= 85.406  
T= .00804 PM1= 180.732 PMDOT= 2020.230 PSI= 24.099 PSINOT= -236.225 PM1101= 85.732  
T= .00805 PM1= 181.058 PMDOT= 2030.642 PSI= 23.964 PSINOT= -236.225 PM1101= 86.058  
T= .00806 PM1= 181.384 PMDOT= 2041.053 PSI= 23.829 PSINOT= -236.225 PM1101= 86.384  
T= .00807 PM1= 181.710 PMDOT= 2051.465 PSI= 23.694 PSINOT= -236.225 PM1101= 86.710  
T= .00808 PM1= 182.036 PMDOT= 2061.877 PSI= 23.559 PSINOT= -236.225 PM1101= 87.036  
T= .00809 PM1= 182.362 PMDOT= 2072.289 PSI= 23.424 PSINOT= -236.225 PM1101= 87.362  
T= .00810 PM1= 182.688 PMDOT= 2082.700 PSI= 23.289 PSINOT= -236.225 PM1101= 87.688  
T= .00811 PM1= 183.014 PMDOT= 2093.112 PSI= 23.154 PSINOT= -236.225 PM1101= 88.014  
T= .00812 PM1= 183.340 PMDOT= 2103.524 PSI= 23.019 PSINOT= -236.225 PM1101= 88.340  
T= .00813 PM1= 183.666 PMDOT= 2113.936 PSI= 22.884 PSINOT= -236.225 PM1101= 88.666  
T= .00814 PM1= 183.992 PMDOT= 2124.347 PSI= 22.749 PSINOT= -236.225 PM1101= 88.992  
T= .00815 PM1= 184.318 PMDOT= 2134.759 PSI= 22.614 PSINOT= -236.225 PM1101= 89.318  
T= .00816 PM1= 184.644 PMDOT= 2145.171 PSI= 22.479 PSINOT= -236.225 PM1101= 89.644  
T= .00817 PM1= 184.970 PMDOT= 2155.583 PSI= 22.344 PSINOT= -236.225 PM1101= 89.970  
T= .00818 PM1= 185.296 PMDOT= 2165.994 PSI= 22.209 PSINOT= -236.225 PM1101= 90.296  
T= .00819 PM1= 185.622 PMDOT= 2176.406 PSI= 22.074 PSINOT= -236.225 PM1101= 90.622  
T= .00820 PM1= 185.948 PMDOT= 2186.818 PSI= 21.939 PSINOT= -236.225 PM1101= 90.948  
T= .00821 PM1= 186.274 PMDOT= 2197.230 PSI= 21.804 PSINOT= -236.225 PM1101= 91.274  
T= .00822 PM1= 186.600 PMDOT= 2207.642 PSI= 21.669 PSINOT= -236.225 PM1101= 91.600  
T= .00823 PM1= 186.926 PMDOT= 2218.053 PSI= 21.534 PSINOT= -236.225 PM1101= 91.926  
T= .00824 PM1= 187.252 PMDOT= 2228.465 PSI= 21.399 PSINOT= -236.225 PM1101= 92.252  
T= .00825 PM1= 187.578 PMDOT= 2238.877 PSI= 21.264 PSINOT= -236.225 PM1101= 92.578  
T= .00826 PM1= 187.904 PMDOT= 2249.289 PSI= 21.129 PSINOT= -236.225 PM1101= 92.904  
T= .00827 PM1= 188.230 PMDOT= 2259.700 PSI= 20.994 PSINOT= -236.225 PM1101= 93.230  
T= .00828 PM1= 188.556 PMDOT= 2270.112 PSI= 20.859 PSINOT= -236.225 PM1101= 93.556  
T= .00829 PM1= 188.882 PMDOT= 2280.524 PSI= 20.724 PSINOT= -236.225 PM1101= 93.882  
T= .00830 PM1= 189.208 PMDOT= 2290.936 PSI= 20.589 PSINOT= -236.225 PM1101= 94.208  
T= .00831 PM1= 189.534 PMDOT= 2301.347 PSI= 20.4

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NOI 10M 3353

Tz	.01095	PWt	186.763	PmDot	105.444	PSt	311.572	PStDot	192.390	PwDot	51.743
Tz	.01095	PWt	186.807	PmDot	115.856	PSt	311.682	PStDot	192.390	PwDot	51.807
Tz	.01066	PWt	186.876	PmDot	126.268	PSt	311.792	PStDot	192.390	PwDot	51.876
Tz	.01068	PWt	186.951	PmDot	136.680	PSt	311.903	PStDot	192.390	PwDot	51.951
Tz	.01069	PWt	187.033	PmDot	147.092	PSt	312.013	PStDot	192.390	PwDot	52.013
Tz	.01070	PWt	187.123	PmDot	157.503	PSt	312.123	PStDot	192.390	PwDot	52.123
Tz	.01071	PWt	187.213	PmDot	167.915	PSt	312.233	PStDot	192.390	PwDot	52.213
Tz	.01072	PWt	187.312	PmDot	178.327	PSt	312.343	PStDot	192.390	PwDot	52.312
Tz	.01073	PWt	187.418	PmDot	188.739	PSt	312.454	PStDot	192.390	PwDot	52.418
Tz	.01074	PWt	187.529	PmDot	199.150	PSt	312.564	PStDot	192.390	PwDot	52.520
Tz	.01075	PWt	187.655	PmDot	209.562	PSt	312.674	PStDot	192.390	PwDot	52.646
Tz	.01076	PWt	187.769	PmDot	219.974	PSt	312.784	PStDot	192.390	PwDot	52.769
Tz	.01077	PWt	187.898	PmDot	230.386	PSt	312.895	PStDot	192.390	PwDot	52.898
Tz	.01078	PWt	188.033	PmDot	240.797	PSt	313.005	PStDot	192.390	PwDot	53.033
Tz	.01079	PWt	188.174	PmDot	251.209	PSt	313.115	PStDot	192.390	PwDot	53.174
Tz	.01080	PWt	188.321	PmDot	261.621	PSt	313.225	PStDot	192.390	PwDot	53.321
Tz	.01081	PWt	188.474	PmDot	272.033	PSt	313.336	PStDot	192.390	PwDot	53.474
Tz	.01082	PWt	188.632	PmDot	282.444	PSt	313.446	PStDot	192.390	PwDot	53.632
Tz	.01083	PWt	188.797	PmDot	292.856	PSt	313.556	PStDot	192.390	PwDot	53.797
Tz	.01084	PWt	188.968	PmDot	303.268	PSt	313.666	PStDot	192.390	PwDot	53.968
Tz	.01085	PWt	189.165	PmDot	313.680	PSt	313.776	PStDot	192.390	PwDot	54.145
Tz	.01086	PWt	189.327	PmDot	324.092	PSt	313.887	PStDot	192.390	PwDot	54.327
Tz	.01087	PWt	189.515	PmDot	334.503	PSt	313.997	PStDot	192.390	PwDot	54.516
Tz	.01088	PWt	189.711	PmDot	344.915	PSt	314.107	PStDot	192.390	PwDot	54.711
Tz	.01089	PWt	189.911	PmDot	355.327	PSt	314.217	PStDot	192.390	PwDot	54.911
Tz	.01090	PWt	190.118	PmDot	365.739	PSt	314.328	PStDot	192.390	PwDot	55.118
Tz	.01091	PWt	190.330	PmDot	376.150	PSt	314.438	PStDot	192.390	PwDot	55.330
Tz	.01092	PWt	190.549	PmDot	386.562	PSt	314.548	PStDot	192.390	PwDot	55.549
Tz	.01093	PWt	190.773	PmDot	396.974	PSt	314.658	PStDot	192.390	PwDot	55.773
Tz	.01094	PWt	191.004	PmDot	407.386	PSt	314.769	PStDot	192.390	PwDot	56.004
Tz	.01095	PWt	191.240	PmDot	417.797	PSt	314.879	PStDot	192.390	PwDot	56.240
Tz	.01096	PWt	191.483	PmDot	428.209	PSt	314.989	PStDot	192.390	PwDot	56.483
Tz	.01097	PWt	191.731	PmDot	438.621	PSt	315.099	PStDot	192.390	PwDot	56.731
Tz	.01098	PWt	191.985	PmDot	449.033	PSt	315.209	PStDot	192.390	PwDot	56.985
Tz	.01099	PWt	192.245	PmDot	459.444	PSt	315.320	PStDot	192.390	PwDot	57.245
Tz	.01100	PWt	192.512	PmDot	469.856	PSt	315.430	PStDot	192.390	PwDot	57.512
Tz	.01101	PWt	192.784	PmDot	480.268	PSt	315.540	PStDot	192.390	PwDot	57.784

[illegible]

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T= .01334	PMI= 205.657	PHDOIT= 126.871	G= -.0036	GOOT= 31.529	PSIO= 301.266	PSIOOT= 239.559	PMITOT= 71.429
T= .01334	PMI= 206.429	PHDOIT= 132.212	G= -.0004	GOOT= 32.047	PSIO= 300.011	PSIOOT= 239.559	PMITOT= 71.429
T= .01354	PMI= 207.171	PHDOIT= 126.961	G= .0029	GOOT= 32.511	PSIO= 298.620	PSIOOT= 245.981	PMITOT= 72.171
FREE MOTION							
T= .01354	PMI= 127.171	PHDOIT= 126.961	PSI= 47.957	PSIOOT= 245.981	PMITOT= 72.171		
T= .01355	PMI= 127.247	PHDOIT= 137.372	PSI= 47.414	PSIOOT= 245.981	PMITOT= 72.247		
T= .01356	PMI= 127.329	PHDOIT= 147.746	PSI= 47.875	PSIOOT= 245.981	PMITOT= 72.329		
T= .01357	PMI= 127.416	PHDOIT= 158.196	PSI= 47.334	PSIOOT= 245.981	PMITOT= 72.416		
T= .01358	PMI= 127.510	PHDOIT= 168.608	PSI= 47.393	PSIOOT= 245.981	PMITOT= 72.510		
T= .01359	PMI= 127.610	PHDOIT= 179.019	PSI= 47.252	PSIOOT= 245.981	PMITOT= 72.610		
T= .01360	PMI= 127.715	PHDOIT= 189.431	PSI= 47.111	PSIOOT= 245.981	PMITOT= 72.715		
T= .01361	PMI= 127.827	PHDOIT= 199.843	PSI= 46.970	PSIOOT= 245.981	PMITOT= 72.827		
T= .01362	PMI= 127.944	PHDOIT= 210.255	PSI= 46.829	PSIOOT= 245.981	PMITOT= 72.944		
T= .01363	PMI= 128.068	PHDOIT= 220.667	PSI= 46.688	PSIOOT= 245.981	PMITOT= 73.068		
T= .01364	PMI= 128.197	PHDOIT= 231.078	PSI= 46.547	PSIOOT= 245.981	PMITOT= 73.197		
T= .01365	PMI= 128.332	PHDOIT= 241.490	PSI= 46.406	PSIOOT= 245.981	PMITOT= 73.332		
T= .01366	PMI= 128.474	PHDOIT= 251.902	PSI= 46.264	PSIOOT= 245.981	PMITOT= 73.474		
T= .01367	PMI= 128.621	PHDOIT= 262.314	PSI= 46.123	PSIOOT= 245.981	PMITOT= 73.621		
T= .01368	PMI= 128.774	PHDOIT= 272.725	PSI= 45.984	PSIOOT= 245.981	PMITOT= 73.774		
T= .01369	PMI= 128.934	PHDOIT= 283.137	PSI= 45.843	PSIOOT= 245.981	PMITOT= 73.934		
T= .01370	PMI= 129.099	PHDOIT= 293.549	PSI= 45.702	PSIOOT= 245.981	PMITOT= 74.099		
T= .01371	PMI= 129.270	PHDOIT= 303.961	PSI= 45.561	PSIOOT= 245.981	PMITOT= 74.270		
T= .01372	PMI= 129.447	PHDOIT= 314.372	PSI= 45.420	PSIOOT= 245.981	PMITOT= 74.447		
T= .01373	PMI= 129.630	PHDOIT= 324.784	PSI= 45.279	PSIOOT= 245.981	PMITOT= 74.630		
T= .01374	PMI= 129.819	PHDOIT= 335.196	PSI= 45.138	PSIOOT= 245.981	PMITOT= 74.819		
T= .01375	PMI= 130.014	PHDOIT= 345.608	PSI= 44.997	PSIOOT= 245.981	PMITOT= 75.014		
T= .01376	PMI= 130.215	PHDOIT= 356.019	PSI= 44.856	PSIOOT= 245.981	PMITOT= 75.215		
T= .01377	PMI= 130.422	PHDOIT= 366.431	PSI= 44.715	PSIOOT= 245.981	PMITOT= 75.422		
T= .01378	PMI= 130.635	PHDOIT= 376.843	PSI= 44.574	PSIOOT= 245.981	PMITOT= 75.635		
T= .01379	PMI= 130.854	PHDOIT= 387.255	PSI= 44.433	PSIOOT= 245.981	PMITOT= 75.854		
T= .01380	PMI= 131.079	PHDOIT= 397.667	PSI= 44.292	PSIOOT= 245.981	PMITOT= 76.079		
T= .01381	PMI= 131.310	PHDOIT= 408.078	PSI= 44.152	PSIOOT= 245.981	PMITOT= 76.310		
T= .01382	PMI= 131.547	PHDOIT= 418.490	PSI= 44.011	PSIOOT= 245.981	PMITOT= 76.547		
T= .01383	PMI= 131.789	PHDOIT= 428.902	PSI= 43.870	PSIOOT= 245.981	PMITOT= 76.789		
T= .01384	PMI= 132.038	PHDOIT= 439.314	PSI= 43.729	PSIOOT= 245.981	PMITOT= 77.038		
T= .01385	PMI= 132.293	PHDOIT= 449.725	PSI= 43.588	PSIOOT= 245.981	PMITOT= 77.293		
T= .01386	PMI= 132.553	PHDOIT= 460.137	PSI= 43.447	PSIOOT= 245.981	PMITOT= 77.553		
T= .01387	PMI= 132.820	PHDOIT= 470.549	PSI= 43.306	PSIOOT= 245.981	PMITOT= 77.820		
T= .01388	PMI= 133.093	PHDOIT= 480.961	PSI= 43.165	PSIOOT= 245.981	PMITOT= 78.093		
T= .01389	PMI= 133.371	PHDOIT= 491.372	PSI= 43.024	PSIOOT= 245.981	PMITOT= 78.371		
T= .01390	PMI= 133.656	PHDOIT= 501.784	PSI= 42.883	PSIOOT= 245.981	PMITOT= 78.656		
T= .01391	PMI= 133.946	PHDOIT= 512.196	PSI= 42.742	PSIOOT= 245.981	PMITOT= 78.946		
T= .01392	PMI= 134.243	PHDOIT= 522.608	PSI= 42.601	PSIOOT= 245.981	PMITOT= 79.243		
T= .01393	PMI= 134.545	PHDOIT= 533.019	PSI= 42.460	PSIOOT= 245.981	PMITOT= 79.545		
T= .01394	PMI= 134.853	PHDOIT= 543.431	PSI= 42.319	PSIOOT= 245.981	PMITOT= 79.853		
T= .01395	PMI= 135.168	PHDOIT= 553.843	PSI= 42.178	PSIOOT= 245.981	PMITOT= 80.168		
VP= -14.318	VS= 42.251						
IMPACT Cycle No. 3							
VP= -8.773	VS= -8.773	PMI= 135.168	PSI= 42.178	OPMIF= -115.001	PSIO= 42.620	PSIOOT= -14.963	PMITOT= 80.168
COUPLED MOTION							
T= .01395	PMI= 135.168	PHDOIT= -115.001	G= -.0450	GOOT= -24.727	PSIO= 42.620	PSIOOT= -14.963	PMITOT= 80.168
T= .01405	PMI= 136.567	PHDOIT= -96.240	G= -.0473	GOOT= -20.043	PSIO= 41.861	PSIOOT= -114.939	PMITOT= 79.567
T= .01415	PMI= 137.092	PHDOIT= -71.470	G= -.0498	GOOT= -15.046	PSIO= 41.267	PSIOOT= -84.311	PMITOT= 78.042
T= .01425	PMI= 137.751	PHDOIT= -47.064	G= -.0503	GOOT= -9.455	PSIO= 40.859	PSIOOT= -57.244	PMITOT= 76.751
T= .01435	PMI= 138.555	PHDOIT= -21.495	G= -.0511	GOOT= -4.443	PSIO= 40.611	PSIOOT= -26.901	PMITOT= 74.555
T= .01437	PMI= 139.512	PHDOIT= -14.987	G= -.0512	GOOT= -3.174	PSIO= 40.560	PSIOOT= -15.043	PMITOT= 74.524
T= .01440	PMI= 139.512	PHDOIT= -8.450	G= -.0512	GOOT= -1.743	PSIO= 40.554	PSIOOT= -10.174	PMITOT= 78.512
T= .01441	PMI= 139.507	PHDOIT= -5.190	G= -.0512	GOOT= -1.041	PSIO= 40.551	PSIOOT= -6.230	PMITOT= 78.504
T= .01442	PMI= 139.507	PHDOIT= -1.917	G= -.0512	GOOT= -.399	PSIO= 40.551	PSIOOT= -2.304	PMITOT= 78.504
T= .01443	PMI= 139.504	PHDOIT= -1.004	G= -.0512	GOOT= -.229	PSIO= 40.551	PSIOOT= -1.321	PMITOT= 78.504
T= .01443	PMI= 139.504	PHDOIT= -.280	G= -.0512	GOOT= -.058	PSIO= 40.551	PSIOOT= -.337	PMITOT= 78.504

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1= .05027	PHI= 134.310	PH001= 544.586	PSI= 43.636	PSI001= 235.683	PHI001= 279.625	PHI001= 279.625
1= .05028	PHI= 134.625	PH001= 554.998	PSI= 43.497	PSI001= 235.683	PHI001= 279.625	PHI001= 279.625
1= .05029	PHI= 134.625	PH001= 565.410	PSI= 43.382	PSI001= 235.683	PHI001= 279.625	PHI001= 279.625
1= .05030	PHI= 135.273	PH001= 575.822	PSI= 43.227	PSI001= 235.683	PHI001= 279.625	PHI001= 279.625
1= .05031	PHI= 135.606	PH001= 586.233	PSI= 43.092	PSI001= 235.683	PHI001= 279.625	PHI001= 279.625
VP= -13.887	VS= 45.689					
IMPACT						
Cycle No. 8						
VP= -8.178	VS= -8.138	DPHIF= -104.424	PSI= 43.092	DPHIF= -134.107	PHI001= 280.606	
COUPLED MOTION						
1= .05031	PHI= 135.606	PHI001= -104.424	G=	GOOT= -22.476	PSI001= -137.765	PHI001= 280.606
1= .05041	PHI= 135.064	PHI001= -84.234	G=	GOOT= -14.078	PSI001= -104.431	PHI001= 280.606
1= .05051	PHI= 134.644	PHI001= -62.364	G=	GOOT= -8.242	PSI001= -74.973	PHI001= 279.644
1= .05061	PHI= 134.352	PHI001= -39.154	G=	GOOT= -4.293	PSI001= -44.941	PHI001= 279.352
1= .05071	PHI= 134.197	PHI001= -15.047	G=	GOOT= -3.174	PSI001= -14.474	PHI001= 279.197
1= .05073	PHI= 134.179	PHI001= -8.944	G=	GOOT= -1.884	PSI001= -11.394	PHI001= 279.179
1= .05076	PHI= 134.171	PHI001= -2.828	G=	GOOT= -.567	PSI001= -3.586	PHI001= 279.171
1= .05076	PHI= 134.171	PHI001= -2.061	G=	GOOT= -.447	PSI001= -2.558	PHI001= 279.171
1= .05077	PHI= 134.170	PHI001= -1.294	G=	GOOT= -.274	PSI001= -1.409	PHI001= 279.170
1= .05077	PHI= 134.170	PHI001= -.915	G=	GOOT= -.193	PSI001= -1.135	PHI001= 279.170
1= .05077	PHI= 134.170	PHI001= -.533	G=	GOOT= -.112	PSI001= -.860	PHI001= 279.170
1= .05077	PHI= 134.170	PHI001= -.159	G=	GOOT= -.072	PSI001= -.586	PHI001= 279.170
1= .05077	PHI= 134.170	PHI001= -.159	G=	GOOT= -.072	PSI001= -.586	PHI001= 279.170
1= .05077	PHI= 134.170	PHI001= -.221	G=	GOOT= -.047	PSI001= -.274	PHI001= 279.170
1= .05078	PHI= 134.170	PHI001= .289	G=	GOOT= .042	PSI001= .363	PHI001= 279.170
1= .05078	PHI= 134.170	PHI001= .364	G=	GOOT= .077	PSI001= .531	PHI001= 279.170
1= .05078	PHI= 134.170	PHI001= .437	G=	GOOT= .092	PSI001= .539	PHI001= 279.170
1= .05078	PHI= 134.170	PHI001= .576	G=	GOOT= .122	PSI001= .715	PHI001= 279.170
1= .05078	PHI= 134.170	PHI001= .719	G=	GOOT= .152	PSI001= .892	PHI001= 279.170
1= .05079	PHI= 134.171	PHI001= 1.004	G=	GOOT= .212	PSI001= 1.245	PHI001= 279.171
1= .05080	PHI= 134.171	PHI001= 1.284	G=	GOOT= .272	PSI001= 1.594	PHI001= 279.171
1= .05080	PHI= 134.172	PHI001= 1.573	G=	GOOT= .332	PSI001= 1.950	PHI001= 279.172
1= .05081	PHI= 134.172	PHI001= 1.857	G=	GOOT= .392	PSI001= 2.309	PHI001= 279.172
1= .05082	PHI= 134.174	PHI001= 2.424	G=	GOOT= .512	PSI001= 3.009	PHI001= 279.174
1= .05083	PHI= 134.176	PHI001= 2.995	G=	GOOT= .632	PSI001= 3.715	PHI001= 279.176
1= .05085	PHI= 134.178	PHI001= 3.564	G=	GOOT= .752	PSI001= 4.420	PHI001= 279.178
1= .05086	PHI= 134.181	PHI001= 4.133	G=	GOOT= .872	PSI001= 5.126	PHI001= 279.181
1= .05091	PHI= 134.196	PHI001= 5.268	G=	GOOT= 1.112	PSI001= 6.537	PHI001= 279.184
1= .05096	PHI= 134.217	PHI001= 6.403	G=	GOOT= 1.352	PSI001= 7.949	PHI001= 279.196
1= .05101	PHI= 134.240	PHI001= 7.538	G=	GOOT= 1.591	PSI001= 9.361	PHI001= 279.217
1= .05106	PHI= 134.260	PHI001= 8.673	G=	GOOT= 1.831	PSI001= 10.769	PHI001= 279.240
1= .05111	PHI= 134.321	PHI001= 13.166	G=	GOOT= 2.309	PSI001= 13.569	PHI001= 279.240
1= .05121	PHI= 134.422	PHI001= 15.401	G=	GOOT= 2.745	PSI001= 14.504	PHI001= 279.240
1= .05121	PHI= 134.549	PHI001= 18.819	G=	GOOT= 3.240	PSI001= 16.225	PHI001= 279.240
1= .05131	PHI= 134.699	PHI001= 24.144	G=	GOOT= 4.204	PSI001= 24.453	PHI001= 279.242
1= .05141	PHI= 134.873	PHI001= 28.420	G=	GOOT= 5.137	PSI001= 30.471	PHI001= 279.242
1= .05151	PHI= 135.072	PHI001= 32.577	G=	GOOT= 6.069	PSI001= 36.471	PHI001= 279.242
1= .05161	PHI= 135.293	PHI001= 36.623	G=	GOOT= 6.947	PSI001= 41.959	PHI001= 279.242
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1= .05191	PHI= 136.086	PHI001= 48.024	G=	GOOT= 9.599	PSI001= 57.465	PHI001= 279.242
1= .05201	PHI= 136.392	PHI001= 51.544	G=	GOOT= 10.441	PSI001= 62.425	PHI001= 279.242
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1= .05221	PHI= 137.059	PHI001= 58.284	G=	GOOT= 12.049	PSI001= 72.321	PHI001= 279.242
1= .05231	PHI= 137.419	PHI001= 61.343	G=	GOOT= 12.845	PSI001= 77.269	PHI001= 279.242
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1= .05261	PHI= 138.606	PHI001= 70.644	G=	GOOT= 15.245	PSI001= 92.113	PHI001= 279.242
1= .05271	PHI= 139.049	PHI001= 74.273	G=	GOOT= 16.069	PSI001= 97.061	PHI001= 279.242
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1= .05481	PHI= 140.379	PHI001= 126.184	G=	GOOT= 32.000	PSI001= 202.000	PHI001= 279.242
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1= .05521	PHI= 140.379	PHI001= 135.208	G=	GOOT= 35.000	PSI001= 222.000	PHI001= 279.242
1= .05531	PHI= 140.379	PHI001= 137.464	G=	GOOT= 35.747	PSI001= 227.000	PHI001= 279.242
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1= .05581	PHI= 140.379	PHI001= 148.744	G=	GOOT= 39.494	PSI001= 252.000	PHI001= 279.242
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1= .05611	PHI= 140.379	PHI001= 155.511	G=	GOOT= 41.747	PSI001= 267.000	PHI001= 279.242
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1= .05631	PHI= 140.379	PHI001= 160.023	G=	GOOT= 43.241	PSI001= 277.000	PHI001= 279.242
1= .05641	PHI= 140.379	PHI001= 162.279	G=	GOOT= 44.000	PSI001= 282.000	PHI001= 279.242
1= .05651	PHI= 140.379	PHI001= 164.535	G=	GOOT= 44.747	PSI001= 287.000	PHI001= 279.242
1= .05661	PHI= 140.379	PHI001= 166.791	G=	GOOT= 45.494	PSI001= 292.000	PHI001= 279.242
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1= .05721	PHI= 140.379	PHI001= 180.327	G=	GOOT= 50.000	PSI001= 322.000	PHI001= 279.242
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1= .05741	PHI= 140.379	PHI001= 184.839	G=	GOOT= 51.494	PSI001= 332.000	PHI001= 279.242
1= .05751	PHI= 140.379	PHI001= 187.095	G=	GOOT= 52.241	PSI001= 337.000	PHI001= 279.242
1= .05761	PHI= 140.379	PHI001= 189.351	G=	GOOT= 53.000	PSI001= 342.000	PHI001= 279.242
1= .05771	PHI= 140.379	PHI001= 191.607	G=	GOOT= 53.747	PSI001= 347.000	PHI001= 279.242
1= .05781	PHI= 140.379	PHI001= 193.863	G=	GOOT= 54.494	PSI001= 352.000	PHI001= 279.242
1= .05791	PHI= 140.379	PHI001= 196.119	G=	GOOT= 55.241	PSI001= 357.000	PHI001= 279.242
1= .05801	PHI= 140.379	PHI001= 198.375	G=	GOOT= 56.000	PSI001= 362.000	PHI001= 279.242
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PM10IOT	=	287.366
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PM10IOT	=	288.571
PM10IOT	=	289.528
PM10IOT	=	290.096
PM10IOT	=	290.673
PM10IOT	=	291.249
PM10IOT	=	291.857

130.731  
142.511  
146.746  
155.056  
160.325  
165.594  
170.864  
174.138  
181.417  
184.703  
191.998

6	P51D0
1	P51D0
1	P51D0
7	P51D0
4	P51D0
7	P51D0
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7	P51D0
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21.62A  
21.977  
22.511  
23.032  
23.539  
24.036  
24.515  
24.9A3  
25.637

[illegible]

Figure 1. The 12 stimuli used in the experiment. The stimuli were presented in a 2 × 6 grid. The top row shows the stimuli for the 'no' condition, and the bottom row shows the stimuli for the 'yes' condition. The stimuli are arranged in a 2 × 6 grid, with the top row showing the 'no' condition and the bottom row showing the 'yes' condition. The stimuli are arranged in a 2 × 6 grid, with the top row showing the 'no' condition and the bottom row showing the 'yes' condition.

106.99	99.87	94.74	90.67	85.66	80.65
103.31	98.11	94.31	90.67	85.66	80.65
101.50	99.87	94.74	90.67	85.66	80.65

157	PHIL
158	PHIL
159	PHIL
160	PHIL
161	PHIL
162	PHIL
163	PHIL
164	PHIL
165	PHIL
166	PHIL
167	PHIL
168	PHIL
169	PHIL
170	PHIL

[illegible]

22	05321
23	05331
24	05341
25	05351
26	05361
27	05371
28	05381
29	05391
30	05401
31	05411
32	05421
33	05431

PA1TOT	291.455
PA1TOT	291.920
PA1TOT	291.989
PA1TOT	292.064
PA1TOT	292.145
PA1TOT	292.232
PA1TOT	292.375
PA1TOT	292.474
PA1TOT	292.529
PA1TOT	292.640
PA1TOT	292.757
PA1TOT	292.879
PA1TOT	293.004
PA1TOT	293.163
PA1TOT	293.294
PA1TOT	293.435
PA1TOT	293.563
PA1TOT	293.741
PA1TOT	293.906
PA1TOT	294.076
PA1TOT	294.253
PA1TOT	294.435
PA1TOT	294.624
PA1TOT	294.814
PA1TOT	295.019
PA1TOT	295.225
PA1TOT	295.437
PA1TOT	295.655
PA1TOT	295.880
PA1TOT	296.110
PA1TOT	296.346
PA1TOT	296.588
PA1TOT	296.836
PA1TOT	297.090
PA1TOT	297.350
PA1TOT	297.616
PA1TOT	297.888
PA1TOT	298.166
PA1TOT	298.450

951030	191.998
951001	191.998
950303	191.998
100154	191.998
100156	191.998
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100191	191.998
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100197	191.998
100198	191.998
100199	191.998
100200	191.998

[illegible]

146.857	P4001s
146.920	P4001s
146.989	P4001s
147.064	P4001s
147.155	P4001s
147.232	P4001s
147.325	P4001s
147.424	P4001s
147.529	P4001s
147.650	P4001s
147.757	P4001s
147.879	P4001s
148.008	P4001s
148.143	P4001s
148.284	P4001s
148.430	P4001s
148.583	P4001s
148.741	P4001s
148.906	P4001s
149.077	P4001s
149.253	P4001s
149.435	P4001s
149.624	P4001s
149.818	P4001s
150.019	P4001s
150.225	P4001s
150.437	P4001s
150.655	P4001s
150.880	P4001s
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151.366	P4001s
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151.836	P4001s
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[illegible]

057107# 298.450

67-938

7-927 P513 315.9

107-450 DPWF=

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4  
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7  
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2

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-1.179  
-.076

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18	6007
23	6007
23	6007
23	6007

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90	PHI
07	PHI
93	PHI
04	PHI

ON  
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PMI = 197

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05494	PMI = 192.884	PMINDI =	-0.137	G =	-0.0423	GOOI =	-0.019	PSID = 316.422	PSIOT =	-0.110	PMIOT = 297.084
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05497	PMI = 192.824	PMINDI =	0.121	G =	-0.0423	GOOI =	0.017	PSID = 316.422	PSIOT =	-0.103	PMIOT = 297.084
05498	PMI = 192.804	PMINDI =	0.183	G =	-0.0423	GOOI =	0.025	PSID = 316.422	PSIOT =	-0.155	PMIOT = 297.084
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05500	PMI = 192.764	PMINDI =	0.308	G =	-0.0423	GOOI =	0.042	PSID = 316.422	PSIOT =	-0.259	PMIOT = 297.084
05501	PMI = 192.744	PMINDI =	0.368	G =	-0.0423	GOOI =	0.051	PSID = 316.422	PSIOT =	-0.312	PMIOT = 297.084
05502	PMI = 192.724	PMINDI =	0.428	G =	-0.0423	GOOI =	0.059	PSID = 316.422	PSIOT =	-0.364	PMIOT = 297.084
05503	PMI = 192.704	PMINDI =	0.488	G =	-0.0423	GOOI =	0.068	PSID = 316.422	PSIOT =	-0.416	PMIOT = 297.084
05504	PMI = 192.684	PMINDI =	0.548	G =	-0.0423	GOOI =	0.075	PSID = 316.422	PSIOT =	-0.468	PMIOT = 297.084
05505	PMI = 192.664	PMINDI =	0.608	G =	-0.0423	GOOI =	0.084	PSID = 316.422	PSIOT =	-0.520	PMIOT = 297.084
05506	PMI = 192.644	PMINDI =	0.668	G =	-0.0423	GOOI =	0.092	PSID = 316.422	PSIOT =	-0.572	PMIOT = 297.084
05507	PMI = 192.624	PMINDI =	0.728	G =	-0.0423	GOOI =	0.101	PSID = 316.422	PSIOT =	-0.624	PMIOT = 297.084
05508	PMI = 192.604	PMINDI =	0.788	G =	-0.0423	GOOI =	0.109	PSID = 316.422	PSIOT =	-0.676	PMIOT = 297.084
05509	PMI = 192.584	PMINDI =	0.848	G =	-0.0423	GOOI =	0.118	PSID = 316.422	PSIOT =	-0.728	PMIOT = 297.084
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05512	PMI = 193.283	PMINDI =	66.164	G =	-0.0413	GOOI =	6.473	PSID = 315.079	PSIOT =	-36.920	PMIOT = 298.243
05513	PMI = 193.426	PMINDI =	53.518	G =	-0.0410	GOOI =	7.572	PSID = 315.955	PSIOT =	-46.549	PMIOT = 298.426
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05515	PMI = 194.200	PMINDI =	81.101	G =	-0.0391	GOOI =	11.651	PSID = 315.271	PSIOT =	-72.836	PMIOT = 299.200
05516	PMI = 194.701	PMINDI =	93.530	G =	-0.0378	GOOI =	13.624	PSID = 314.814	PSIOT =	-85.791	PMIOT = 299.701
05517	PMI = 195.270	PMINDI =	104.874	G =	-0.0363	GOOI =	15.527	PSID = 314.288	PSIOT =	-98.580	PMIOT = 300.270
05518	PMI = 195.900	PMINDI =	115.041	G =	-0.0347	GOOI =	17.352	PSID = 313.687	PSIOT =	-111.170	PMIOT = 300.900
05519	PMI = 196.586	PMINDI =	123.948	G =	-0.0329	GOOI =	19.093	PSID = 313.015	PSIOT =	-123.525	PMIOT = 301.546
05520	PMI = 197.318	PMINDI =	131.534	G =	-0.0309	GOOI =	20.745	PSID = 312.272	PSIOT =	-135.409	PMIOT = 302.318
05521	PMI = 198.090	PMINDI =	137.777	G =	-0.0287	GOOI =	22.393	PSID = 311.461	PSIOT =	-147.384	PMIOT = 303.090
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05523	PMI = 199.723	PMINDI =	146.204	G =	-0.0240	GOOI =	25.124	PSID = 309.642	PSIOT =	-169.459	PMIOT = 304.723
05524	PMI = 200.567	PMINDI =	148.443	G =	-0.0214	GOOI =	26.381	PSID = 308.638	PSIOT =	-180.444	PMIOT = 305.567
05525	PMI = 201.421	PMINDI =	149.424	G =	-0.0187	GOOI =	27.515	PSID = 307.575	PSIOT =	-190.464	PMIOT = 306.421
05526	PMI = 202.277	PMINDI =	149.222	G =	-0.0159	GOOI =	28.544	PSID = 306.454	PSIOT =	-200.470	PMIOT = 307.277
05527	PMI = 203.129	PMINDI =	147.914	G =	-0.0130	GOOI =	29.529	PSID = 305.280	PSIOT =	-209.570	PMIOT = 308.129
05528	PMI = 203.970	PMINDI =	145.591	G =	-0.0100	GOOI =	30.4370	PSID = 304.054	PSIOT =	-218.245	PMIOT = 308.970
05529	PMI = 204.796	PMINDI =	142.350	G =	-0.0078	GOOI =	31.198	PSID = 302.780	PSIOT =	-223.180	PMIOT = 309.796
05530	PMI = 205.600	PMINDI =	138.315	G =	-0.0049	GOOI =	31.746	PSID = 301.461	PSIOT =	-228.964	PMIOT = 310.600
05531	PMI = 206.379	PMINDI =	133.564	G =	-0.0026	GOOI =	32.245	PSID = 300.100	PSIOT =	-234.989	PMIOT = 311.379
05532	PMI = 207.130	PMINDI =	128.220	G =	-0.0027	GOOI =	32.729	PSID = 298.700	PSIOT =	-240.652	PMIOT = 312.130
FREE MOTION	PMI = 127.1	PMINDI =	128.220	PSI =	48.037	PSINDI =	-247.452	PMIOT =	312.130		
05719	PMI = 127.204	PMINDI =	138.631	PSI =	47.895	PSINDI =	-247.452	PMIOT =	312.206		
05720	PMI = 127.249	PMINDI =	140.043	PSI =	47.754	PSINDI =	-247.452	PMIOT =	312.249		
05721	PMI = 127.297	PMINDI =	159.455	PSI =	47.612	PSINDI =	-247.452	PMIOT =	312.377		
05722	PMI = 127.377	PMINDI =	168.867	PSI =	47.470	PSINDI =	-247.452	PMIOT =	312.471		
05723	PMI = 127.572	PMINDI =	180.278	PSI =	47.338	PSINDI =	-247.452	PMIOT =	312.572		
05724	PMI = 127.678	PMINDI =	190.690	PSI =	47.187	PSINDI =	-247.452	PMIOT =	312.678		
05725	PMI = 127.790	PMINDI =	201.102	PSI =	47.045	PSINDI =	-247.452	PMIOT =	312.790		
05726	PMI = 127.908	PMINDI =	211.514	PSI =	46.903	PSINDI =	-247.452	PMIOT =	312.908		
05727	PMI = 128.032	PMINDI =	221.925	PSI =	46.761	PSINDI =	-247.452	PMIOT =	313.032		
05728	PMI = 128.163	PMINDI =	232.337	PSI =	46.619	PSINDI =	-247.452	PMIOT =	313.163		
05729	PMI = 128.303	PMINDI =		PSI =		PSINDI =		PMIOT =			

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IMPACT

PHIOT= 320.156

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